

Conventional e^+ Source Rotation Target R/D

T. Omori (KEK)

On behalf of the Truly Conventional Collaboration

ANL, IHEP, Hiroshima U, U of Tokyo, KEK, DESY, U of Hamburg, CERN

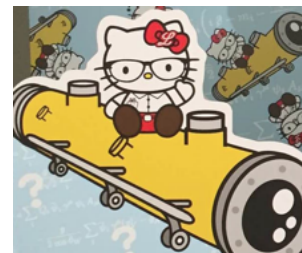
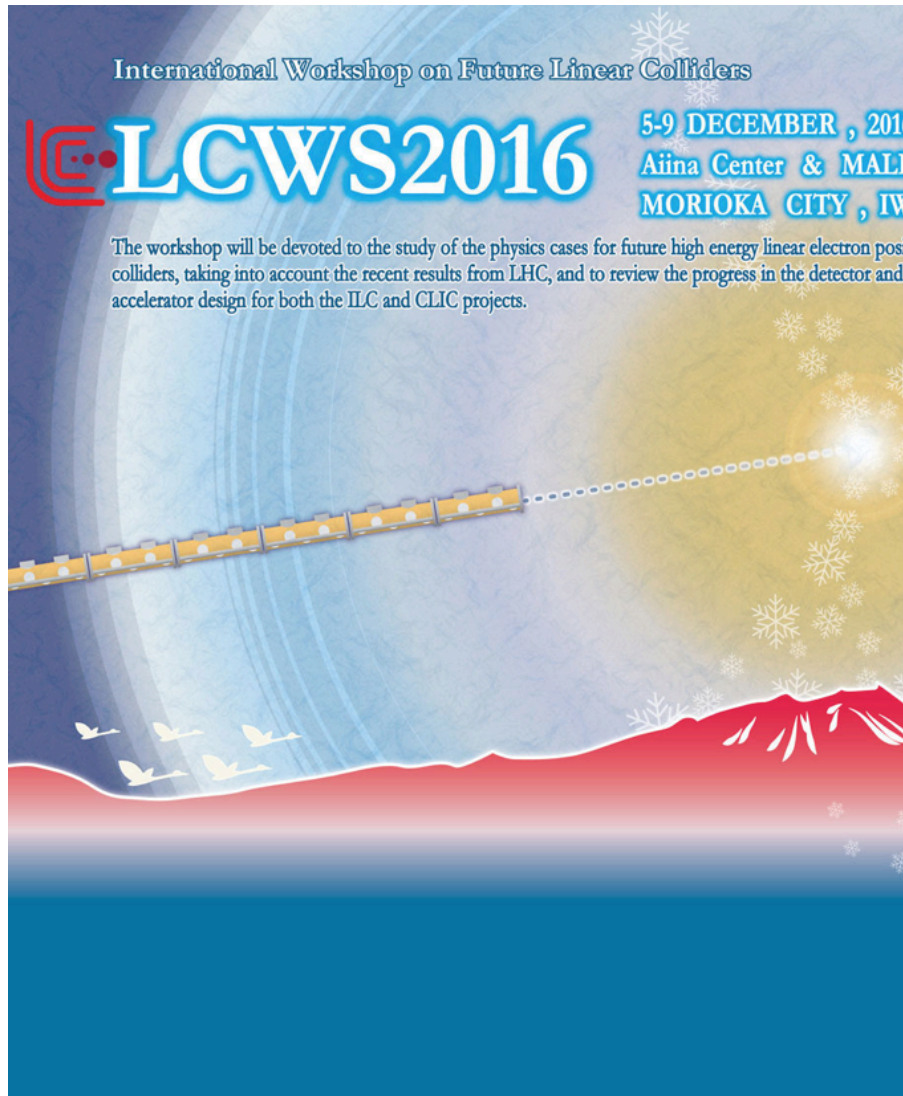
Rotation target design study: ongoing with Rigaku

15-September-2016

Posipol 2016, LAL, Orsay, FRANCE

LCWS 2016

5-9 December, Morioka, Iwate, Japan



The T-shirt and other Kitty Goods will be sold at LCWS 2016.

Plenary Talk by Lyn EVANS

2nd-June-2016 ECFA LCWS Santander, SPAIN



LINEAR COLLIDER COLLABORATION

Nomura report

Only available in Japanese
Weak points identified are
Positron source.
Beam dump.

Today's Talk

R/D of the Slow Rotation Target of the Conventional e^+ Source for ILC

- **Overview**
- **Target R/D (1): Heat and Stress Simulations**
- **Target R/D (2): Radiation, Vacuum, and Prototype**
- **Summary**

Overview

Conventional e+ Source for ILC

Normal Conducting Drive and Booster Linacs in 300 Hz operation

e+ creation

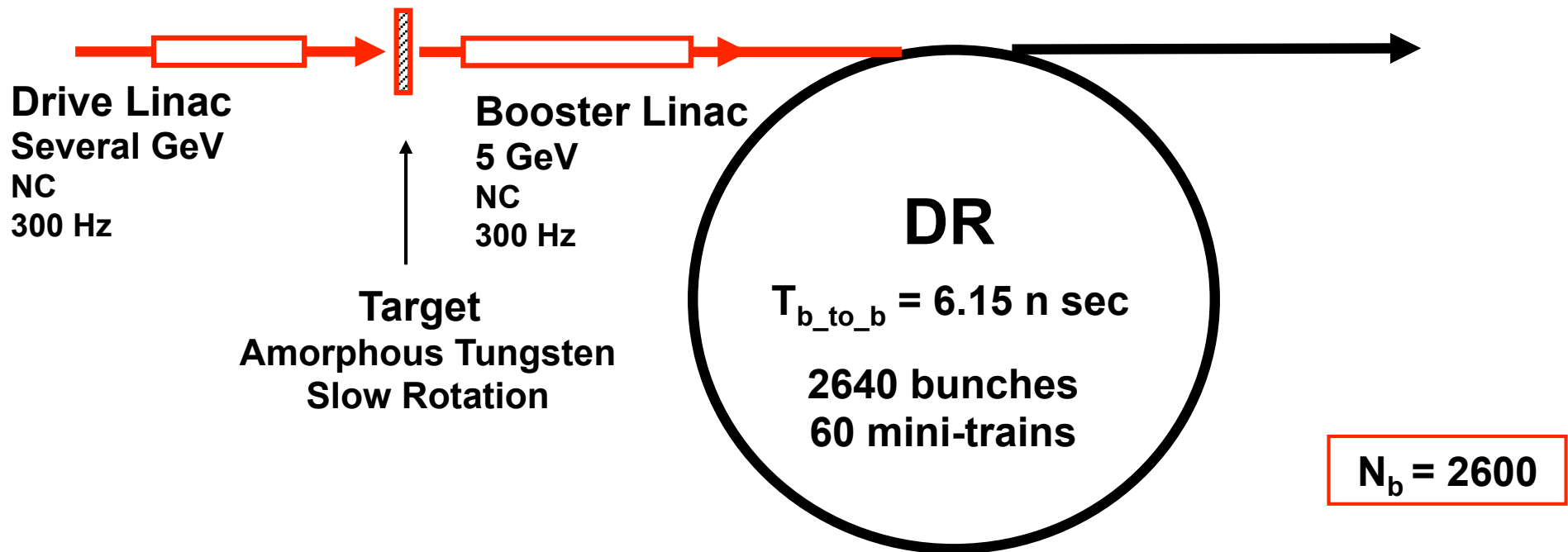
20 triplets, rep. = **300 Hz**

- triplet = 3 mini-trains with gaps
- 44 bunches/mini-train, $T_{b_to_b} = 6.15$ n sec

go to main linac

2640 bunches/train, rep. = 5 Hz

- $T_{b_to_b} = 369$ n sec



Time remaining for damping = **137 m sec**

We create 2640 bunches
in **63 m sec**

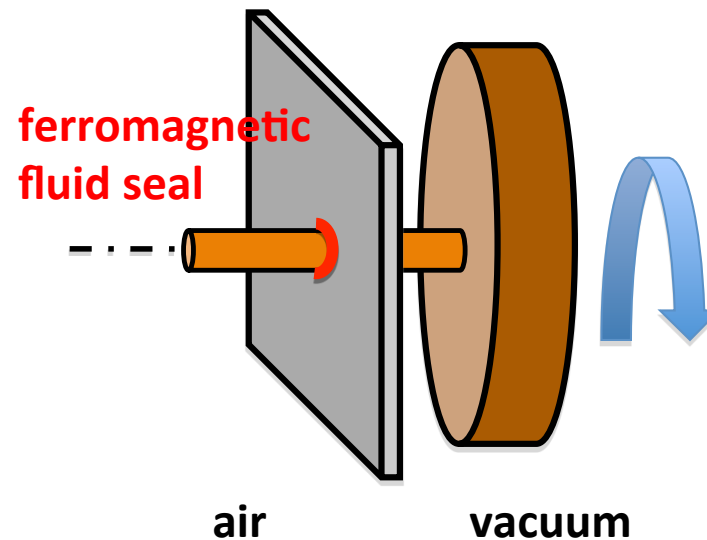
← **Stretching**

NIM A672 (2012) 52—56

Moving Target

- $\sim 5\text{m/sec}$ required (1/20 of undulator scheme)

rotating target with ferromagnetic seal



issues: vacuum, heat, stress

The target R/D (1)

Heat and Stress Simulation

Thermal Analysis:

We did both **CW beam** analysis (for simplicity) and **pulse beam** analysis (more realistic).

We assume **2600 bunches** in all analysis.

- CW beam analysis

38kW (35kW+3kW^(*)) CW
 ↑ ↑
 beam FC

* Note

3 kW is not correct
should be 1 kW

- Pulse beam analysis: **step 1**

114.1 kW(111.1kW+3kW) 63 ms
0 kW (0kW+0kW) 137 ms
 ↑ ↑
 beam FC

- Pulse beam analysis: **step 2**

20 trains (pulses) in 63 ms

- Common condition

$N_b = 2600$

Cooling water: 30 ℓ/min, T at inlet: 25°C



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0 kW (0kW+0kW) 137 ms
↑ ↑
beam FC

Reported
ALCW 2015,
Apr., 2015, Tsukuba
and
Posipol 2015,
Sep., 2015, Daresbury

- **Pulse beam analysis: step 2**

20 trains (pulses) in 63 ms

- **Common condition**

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Cooling water: 30 ℓ/min, T at inlet: 25°C



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- Pulse beam analysis: **step 2**
20 trains (pulses) in 63 ms

Reported
LCWS 2015,
Nov., 2015, Whistler

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Cooling water: 30 ℓ/min, T at inlet: 25°C



Pulse Beam Analysis

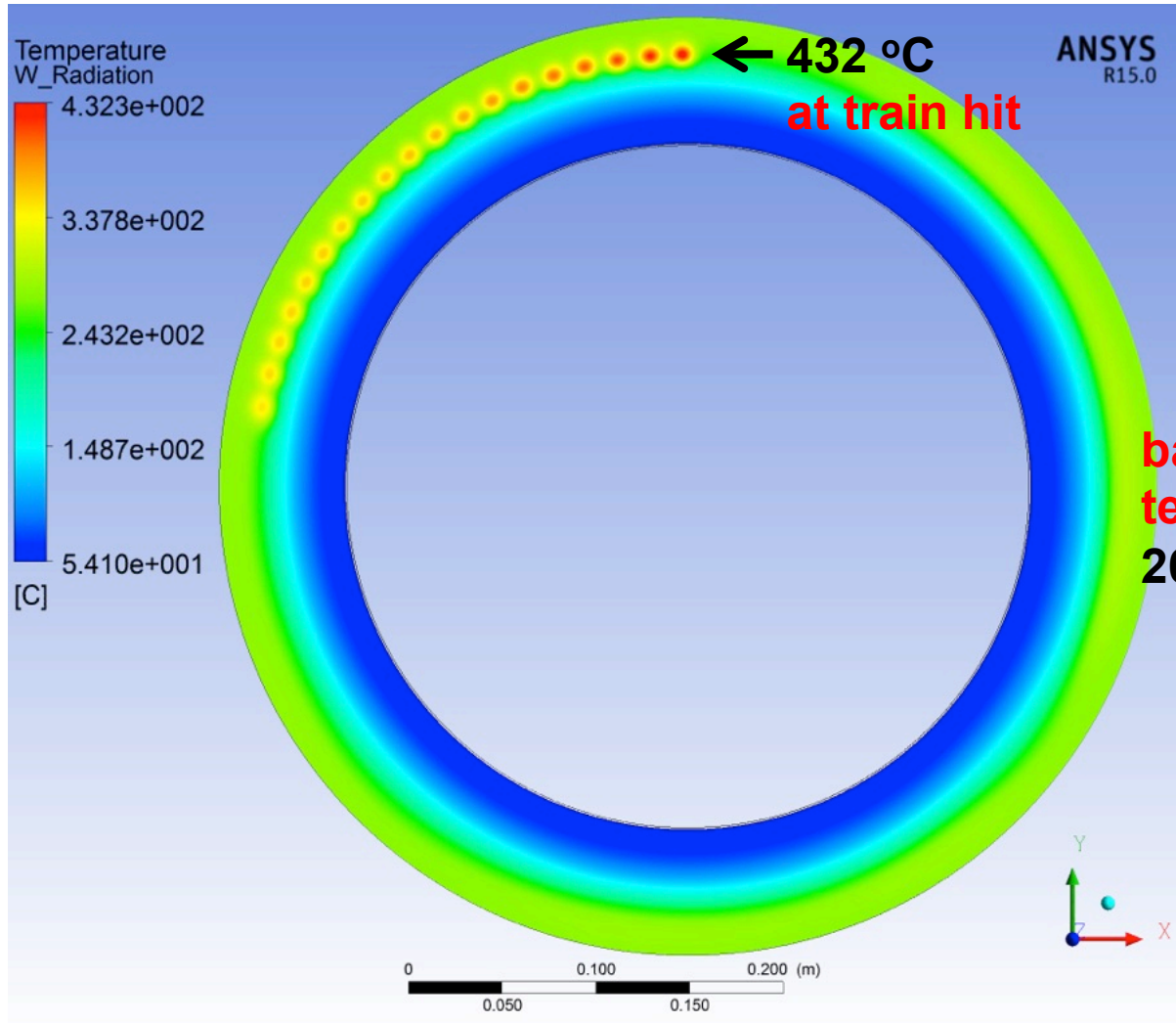
step 2:

20 trains in 63 ms

Rotation speed = **220rpm**

1 train = 373 kW(**) in 0.99 m sec (*)

train to train separation: 3.3 m sec



* Note: 1

One train corresponds 132 bunches, but time structure in a train is ignored.

* Note: 2

This is NOT totally correct.

Pulse width of a train is NOT 0.99 m sec. It is 0.99 micro sec.

But difference in the results are small.

baseline temperature
262 °C

** Note: 3

This value is NOT accurate.

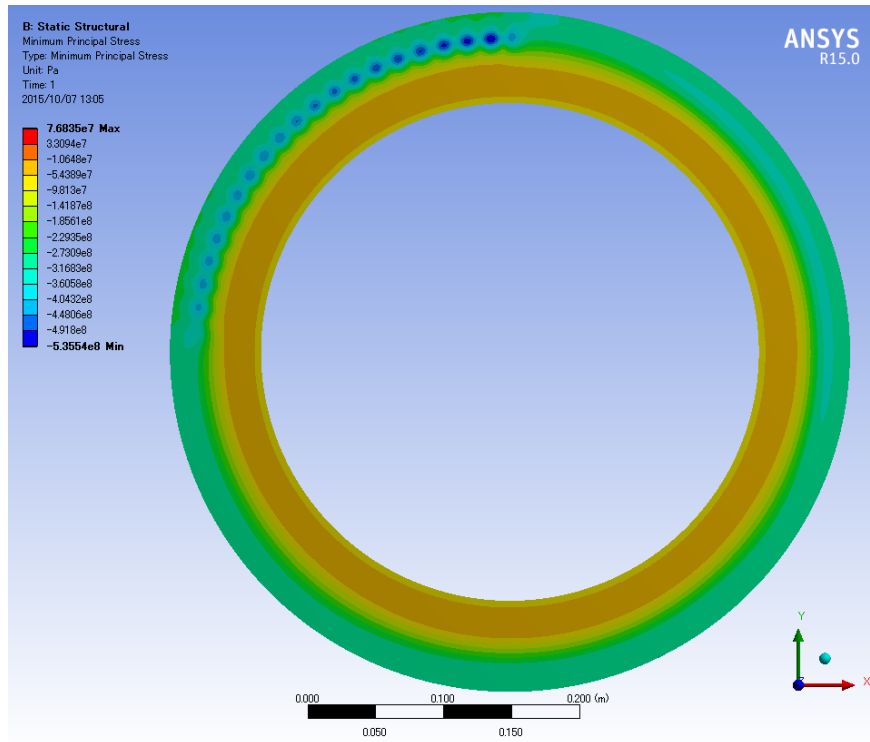
This is 5% larger than correct value.

$N_b = 2600$

Simulated by Rigaku $N_b=2600$

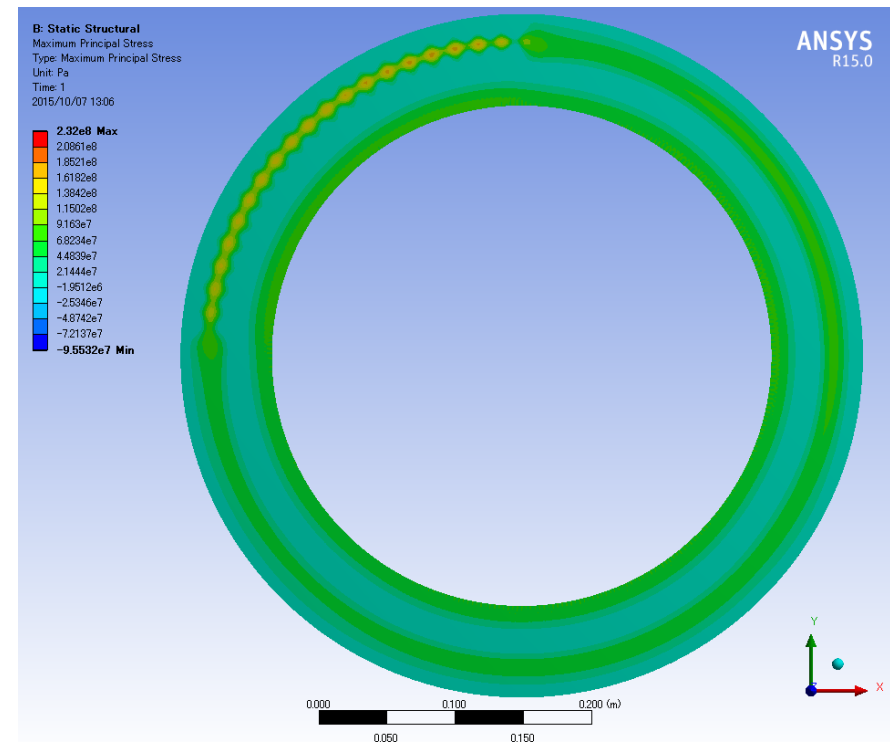
T. Omori, LCWS 2015, 3-Nov-2015, Whistler, CANADA

Stress: rotation speed **220 rpm**, **Pulse Beam Analysis, Step 2** 20 trains in 63 ms



最小主応力
→ $-5.4e+8\text{Pa}$ (圧縮)

Min Principal Stress
(Compression)
→ $-5.4e+8\text{Pa}$



最大主応力
→ $2.3e+8$ (引張り)

Max Principal Stress
(Expansion)
→ $2.3e+8\text{Pa}$

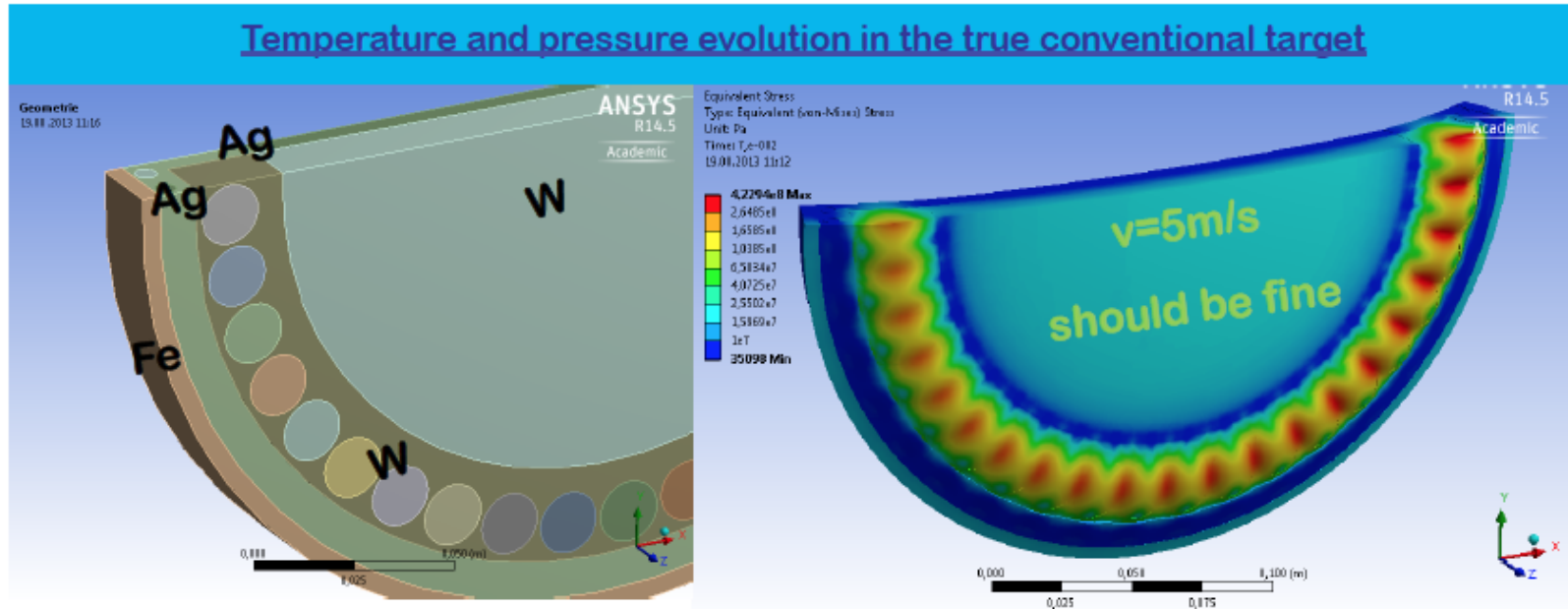
$N_b = 2600$

Simulated by Rigaku

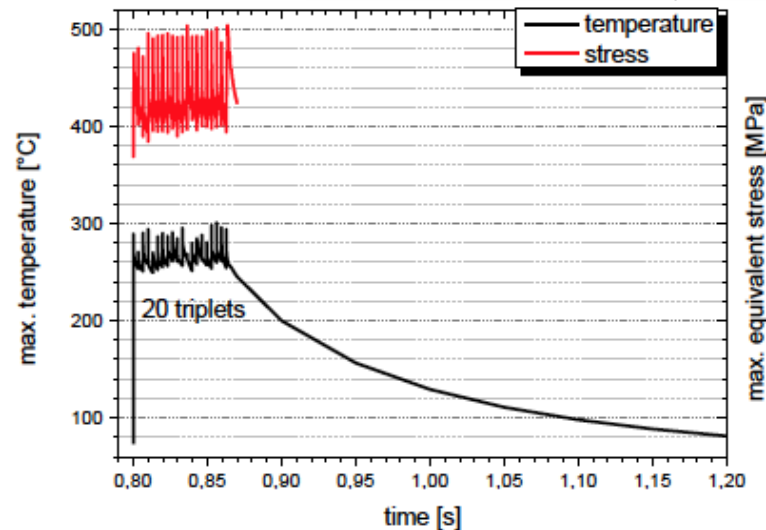
cf. ILC target Analysis by Friedrich-san Posipol 2013, 5th/Sep., at ANL

Max Stress 500 MPa (132 bunches hit the same spot)(Von Mises)

Max 300 度C



cooling : 0.2 l/s
wheel Ø 200mm



**Wheel with v = 5 m/s
should work!!
Beam hits the same
place 2.5 times in a
sec. like the SLAC**

target

**Is ILC Target Safe?
with 540 MPa Peak Stress**

Is ILC Target Safe? with 540 MPa Peak Stress

WRe: Yield Strength and Fatigue Limit

Table 1: WRe structural material properties.

Property	0.0 C	500 C	1000 C
Modulus, Pa	4.3e+11	4.0e+11	3.95e+11
Poisson ratio	0.28	0.28	0.28
Thermal Exp. Coef. 1/C	6.7e-6	7.1e-6	7.95e-6
Yield, Pa	1.6e+9	1.3e+9	9.0e+8

fatigue	640MPa	520MPa	360MPa
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Freidrich Staufenbie, Posipol 2013, 5th/Sep. at ANL

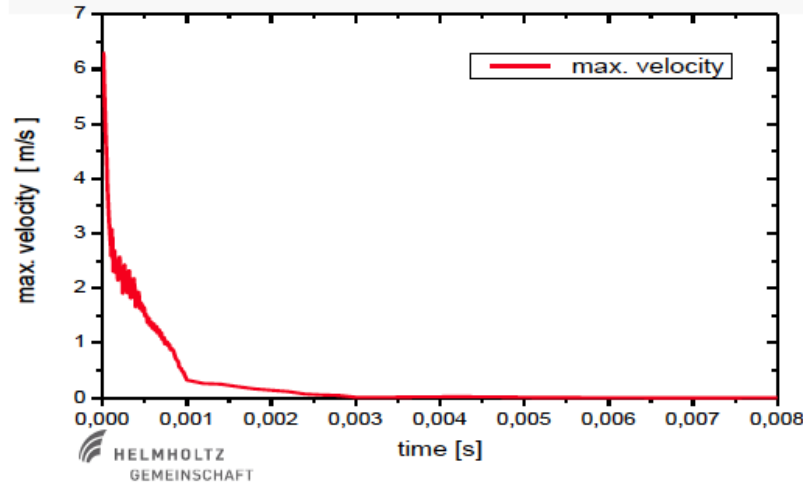
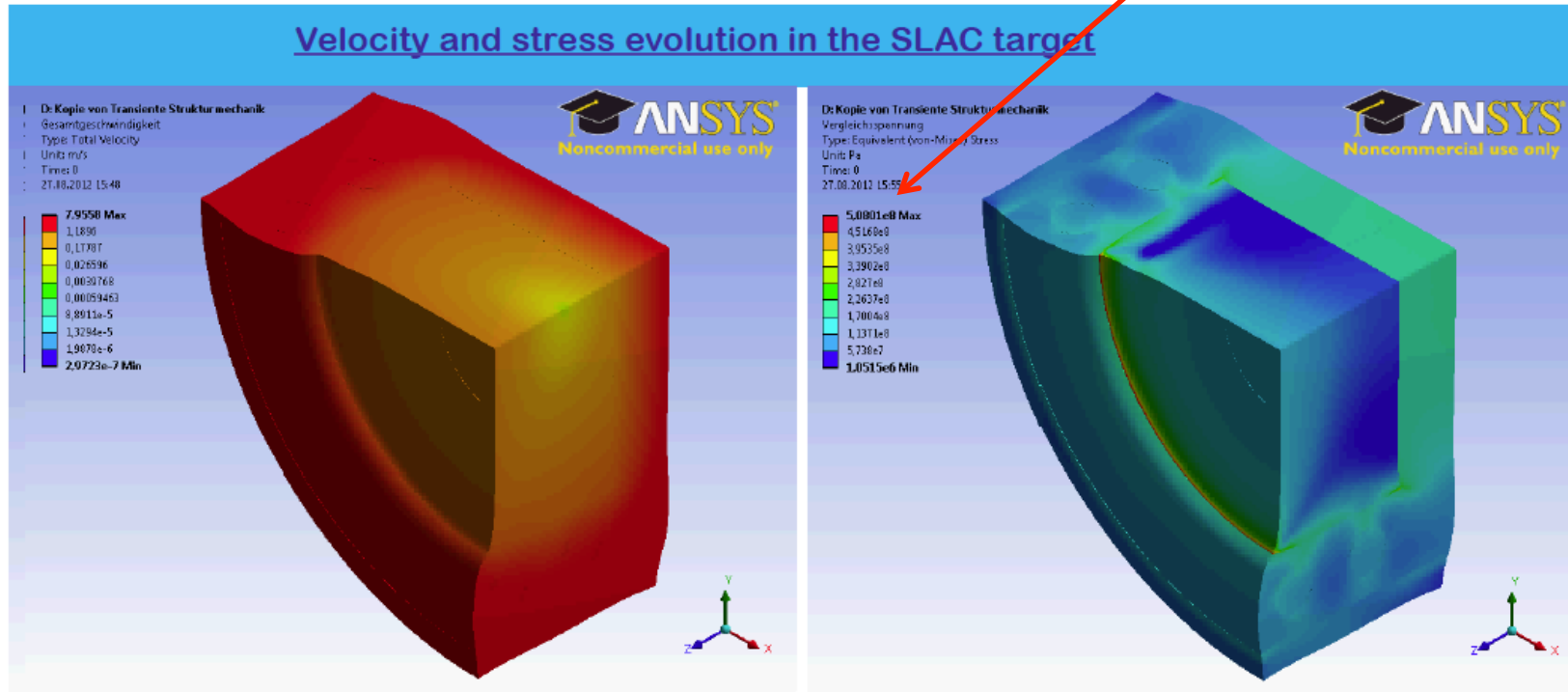
Peak Stress ~ Fatigue Limit

cf. **SLC** target Analysis by Friedrich-san

Posipol 2013, 5th/Sep., at ANL

Max Stress 508 MPa (single bunch)(Von Mises)

Zoom up if you want see the number.



SLAC

33 GeV e⁻
4*10¹⁰ e⁻/pulse (6.4nC)
 $\sigma = 0.8\text{mm}$
120 Hz \approx 8 ms



Is ILC Target Safe?

The greatest achievement so far is the SLC target.

Max stress in the SLC target

508 MPa (analysis by Freidrich-san)

560 MPa (analysis by SLAC, SLAC-PUB-9437)

Max stress in the ILC target

540 MPa (analysis by Rigaku, T. Omori LCWS2015)

SLC target stress and ILC target stress are comparable.

SLC target was destroyed after 3-4 years of operation.

SLC target worked in 3-4 years.

In view point of Max Stress:

ILC target is as safe as SLC target.

Is ILC Target Safe?

Comparison of SLC and ILC

In View Point of Fatigue Effect

PEED	SLC	29 J/g (for 1 bunch)	} comparable
	ILC	27 J/g (for 132 bunches)	

cf. Max Stress of SLC and ILC are comparable. ---> consistent

PEED represents effect of all parameters of the beam and the target; beam energy, spot size, target thickness.

Comparison can be made by number of hits per year.

Beam hits run along the circle.

Compare number of hits per unit length.

(Not per unit area, because PEED already take into account beam spot size.)

Circumferences

SLC: 180mm

ILC: 1500mm

Is ILC Target Safe?

Comparison of SLC and ILC

In View Point of Fatigue Effect

Number of hit / Year.mm

SLC:

$$120 \text{ Hz} \times 3600 \text{ s/h} \times 24 \text{ h/d} \times 365 \text{ d/y} / 180 \text{ mm} = 2.1 \text{ e}+7 \text{ hits/year.mm}$$

ILC:

$$2600/132 \times 5 \text{ Hz} \times 3600 \text{ s/h} \times 24 \text{ h/d} \times 365 \text{ d/y} / 1500 \text{ mm} = 2.1 \text{ e}+6 \text{ hits/year.mm}$$

Def. of hit

SLC: 1 hit = 1 bunch

ILC: 1 hit = 132 bunches

In view point of Number of hit / year.mm;

In the view point of Fatigue;

ILC target (conventional) 10 times ease than SLC target.

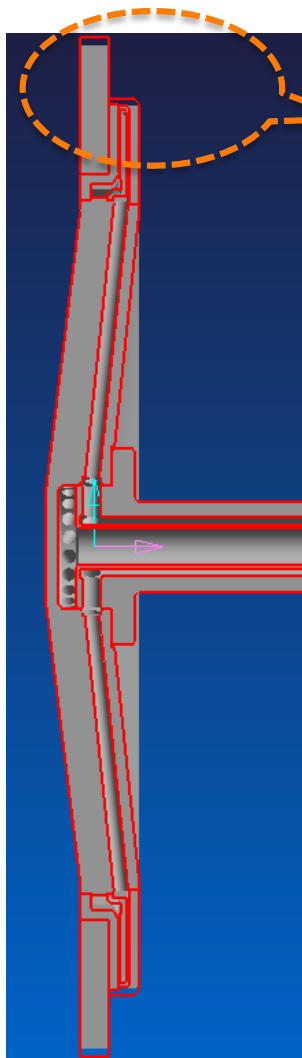
Note: rather rough estimation:

$$N_b = 2600$$

To Get Improved Safety (1)

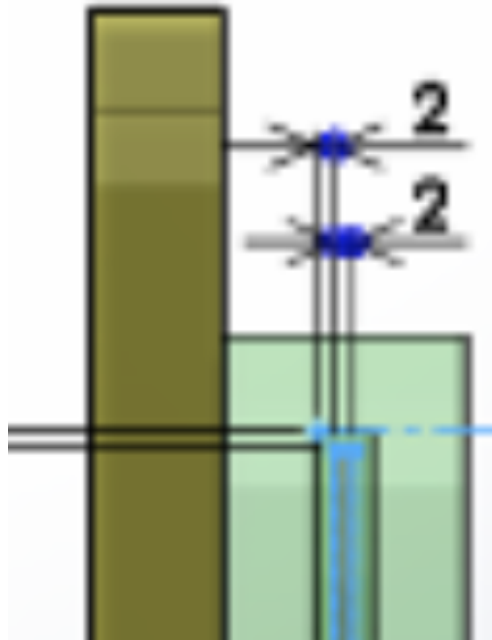
Trying Better Cooling: water channel design

Outline

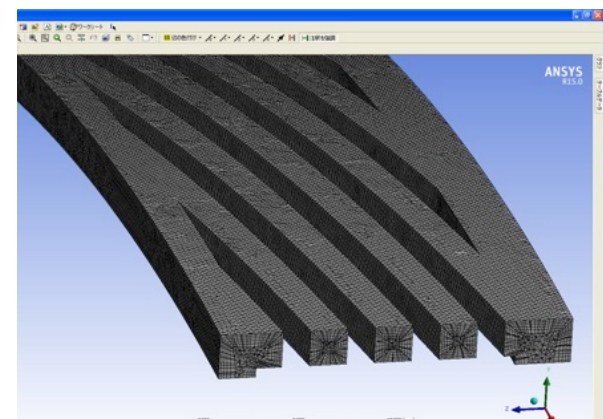
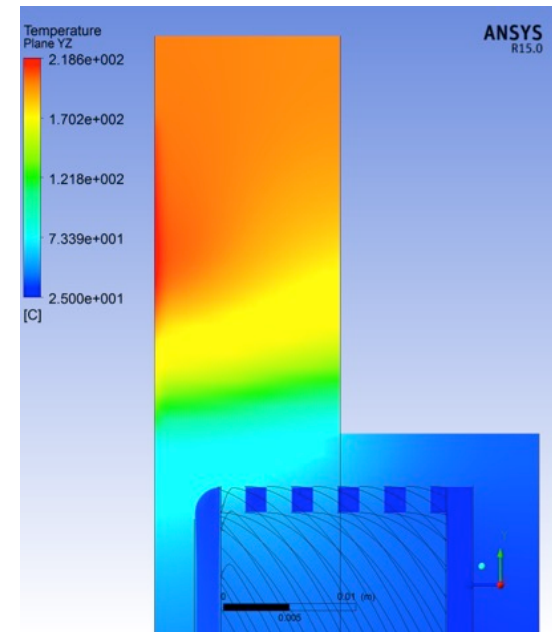


detail

Detail: Old Design
(Model 39)



Detail: New Design
(Model 50)



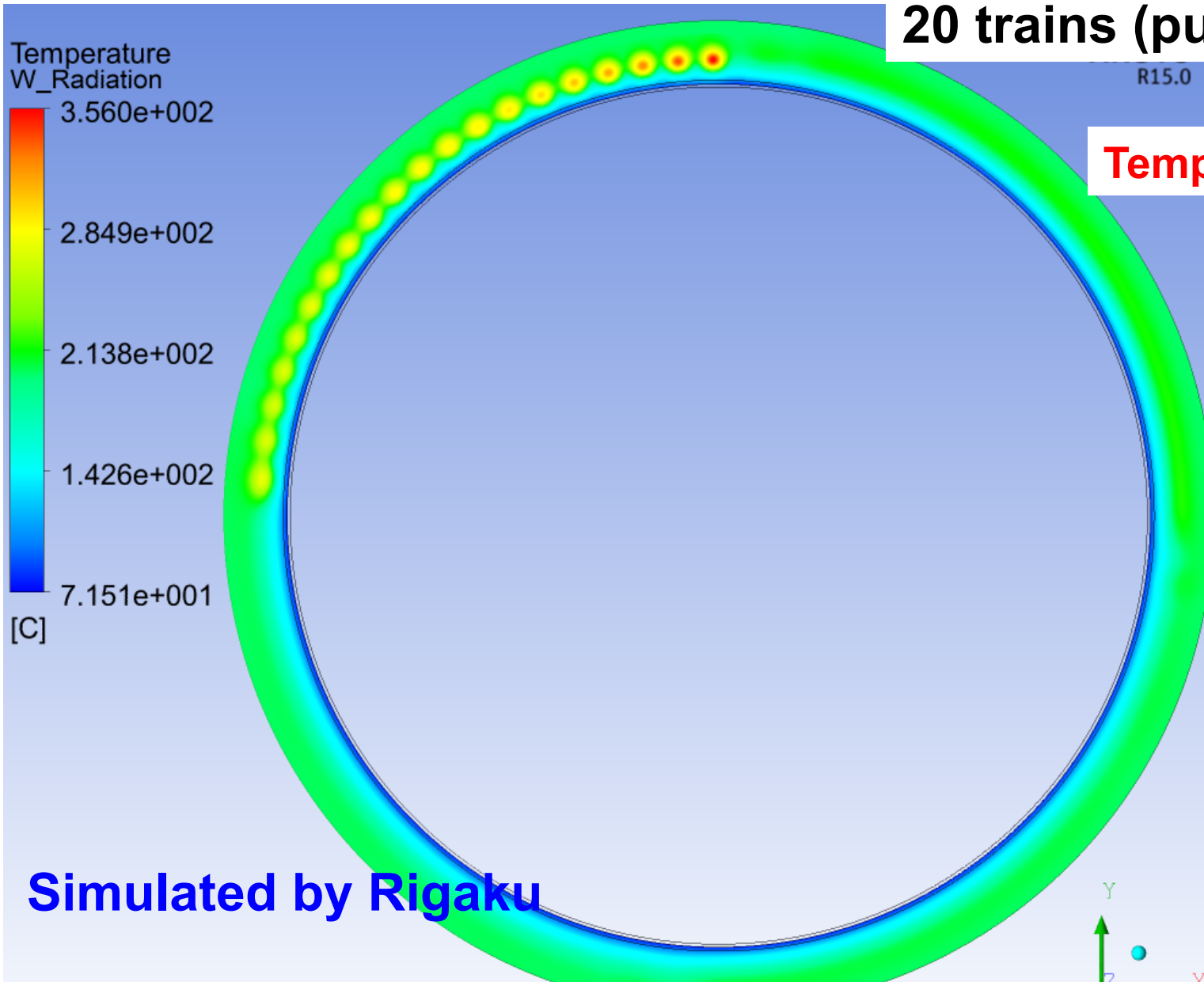
To Get Improved Safety (1)

Trying Better Cooling: water channel design

非定常解析 Pulse#02 225rpm

Pulse beam analysis: step 2

20 trains (pulses) in 63 ms



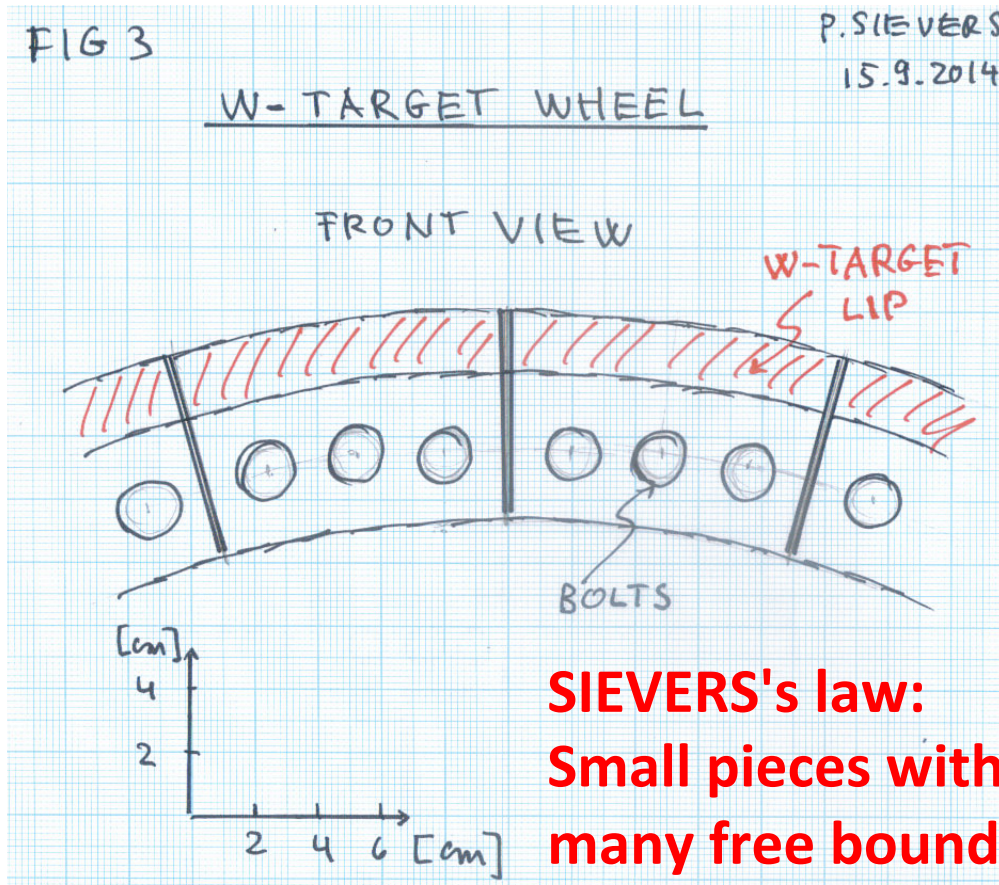
Temp.Max.; 356.0°C

**About 100°C
reduction.
with new water
channel design
in the disk.
(Model 50)**

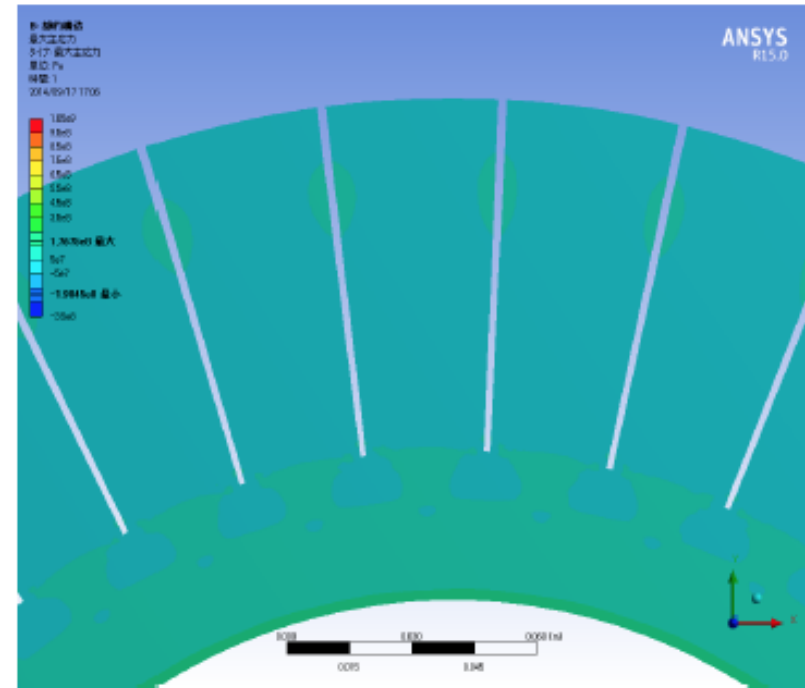
Simulated by Rigaku



To Get Improved Safety We have another room of improvement



SIEVERS's law:
Small pieces with
many free boundaryes
make stresses small.



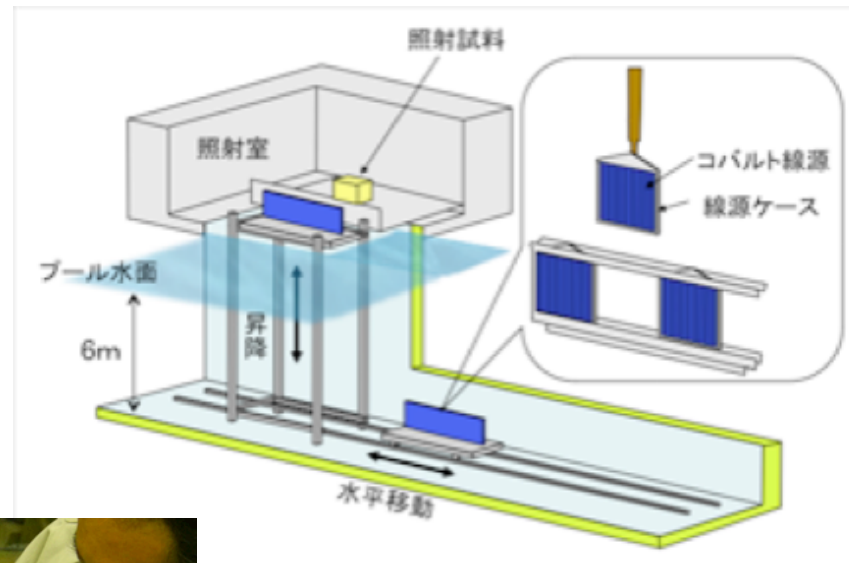
**Target outer disk
with radial slits**

The target R/D (2)

**Radiation Issues,
Vacuum Issues,
and
Prototype Target**

TEST: Radiation Tolerance Mar 2015

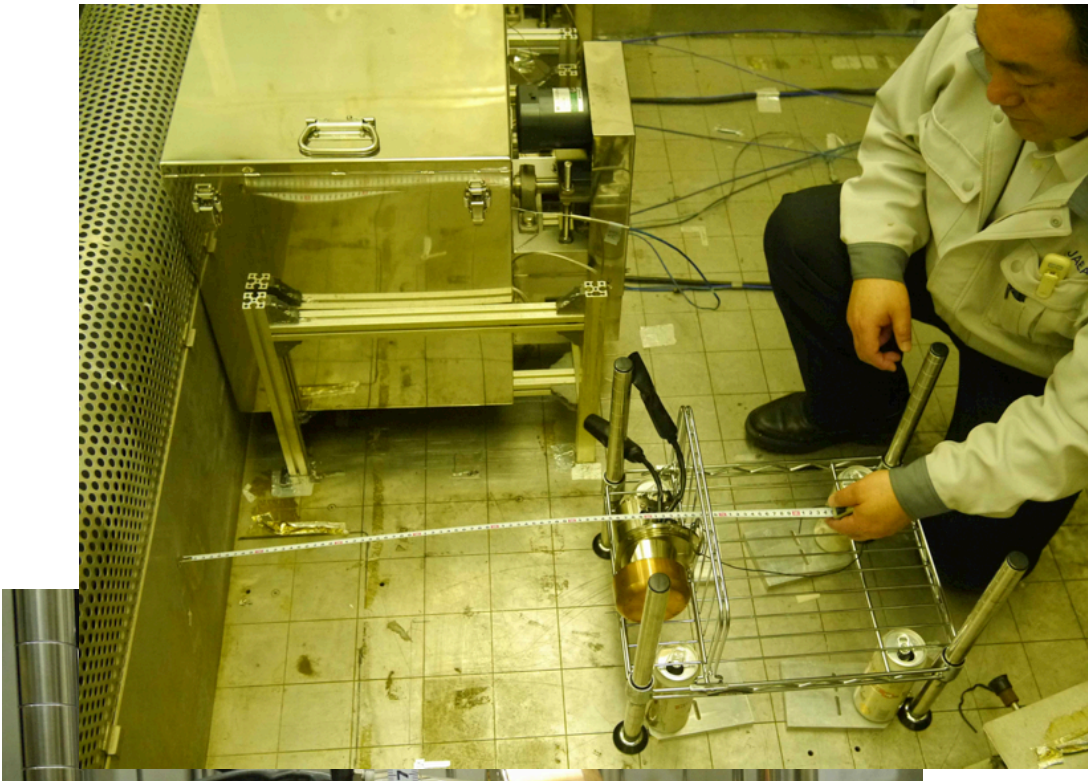
Takasaki Advanced Radiation Research Institute, JAEA



Irradiation to the small ($d=10$ cm) off-the-shelf rotation target.

Radiation test of the
whole system.

cf. ferrofluid test was already done separately upto 4.7 Mgy (3 ILC years).

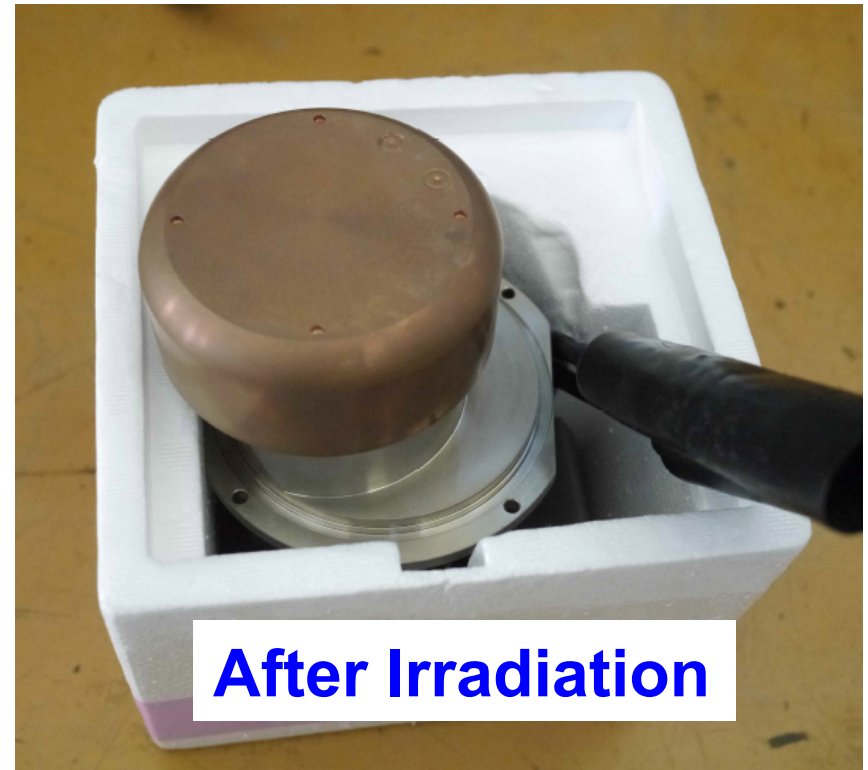
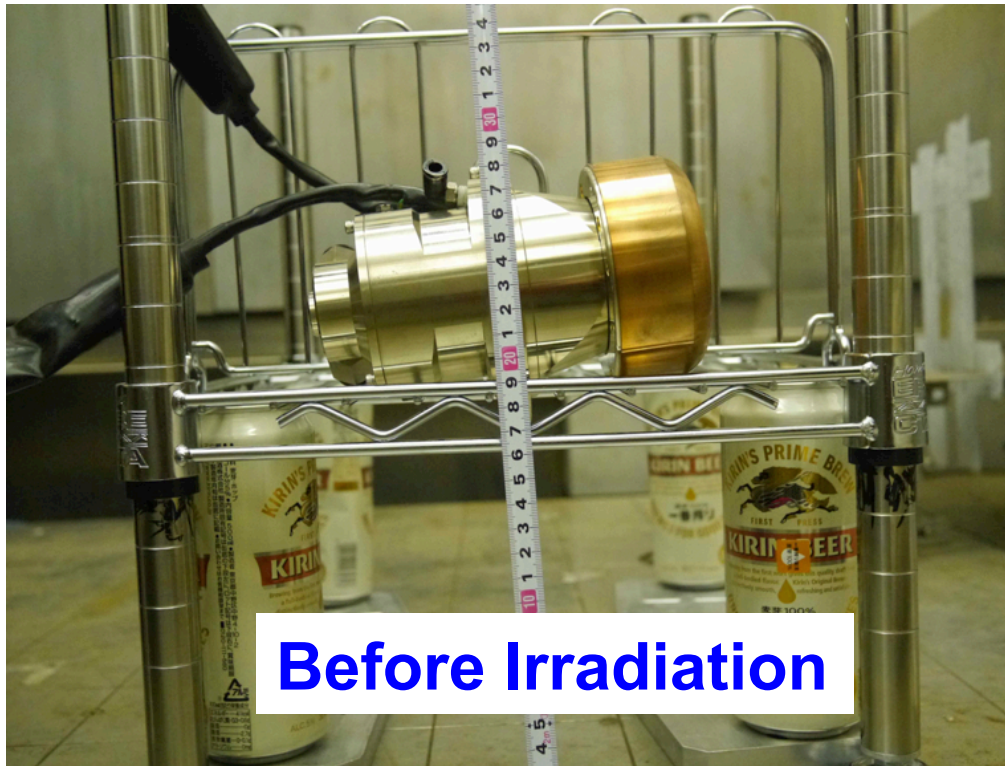


TEST: Radiation Tolerance **Mar 2015**

Irradiation to the small (d=10 cm) off-the-shelf rotation target

Radiation test of the **whole system**: motor, bearing, ferrofluid,,,

0.6 M Gy irradiation on the motor.
corresponds 1 ILC year



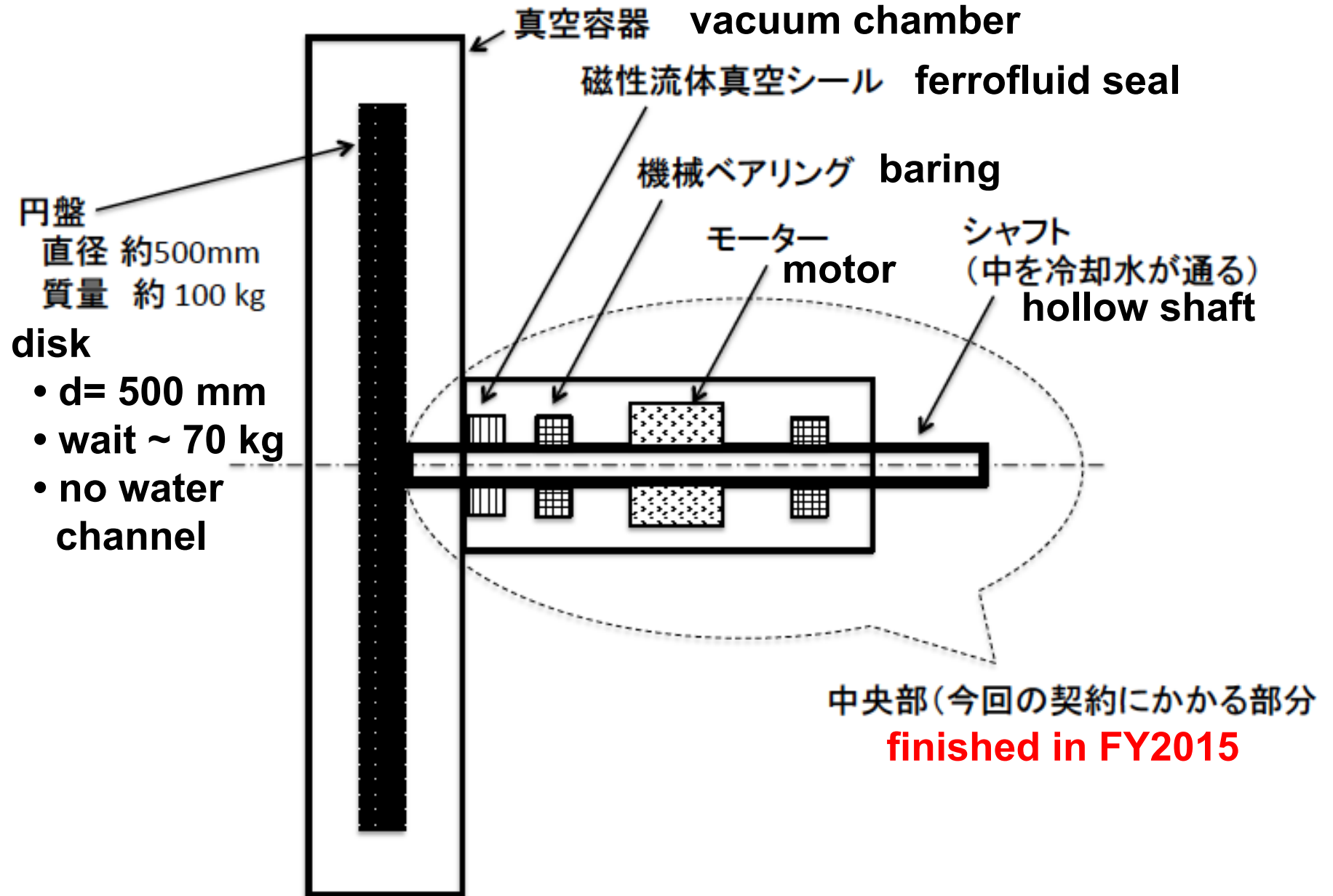
After irradiation, we made **rotation and vacuum** test.

We found NO problem

Plan of Prototpe in FY2015-2017

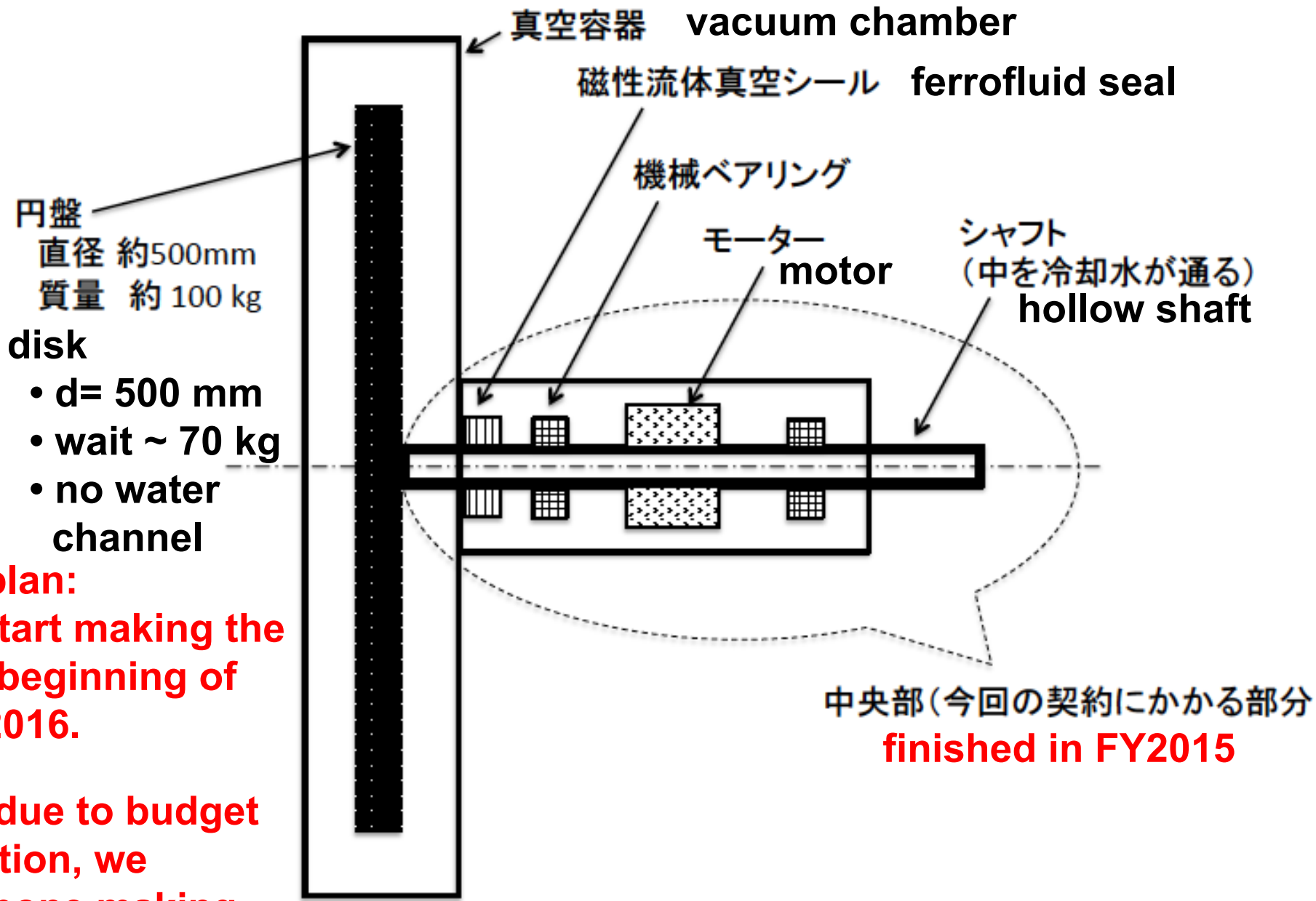
- (1) We are making the prototype in three years (FY2015-2017).
(Old Plan: It was two-year plan in FY2015-FY2016)**
- (2) The prototype is full-size, $d=500$ mm.**
- (3) Full-size means that target wheel has the same radius, the same weight, the same moment as those of the real target. The locations of the vacuum seal and bearing in the prototype are as same as those in the real one.**
- (4) The prototype is not totally as same as the real one.
 - The prototype has no water channels in the disk.
 - We don't use W for disk.**
- (5) We will use irradiated ferromagnetic fluid in the prototype.**
- (6) We will make continuous running test (~1 year?) and will prove that vacuum always stay good level.**

Prototype: We have made a contract with Rigaku.



回転ターゲットプロトタイプ概略断面図

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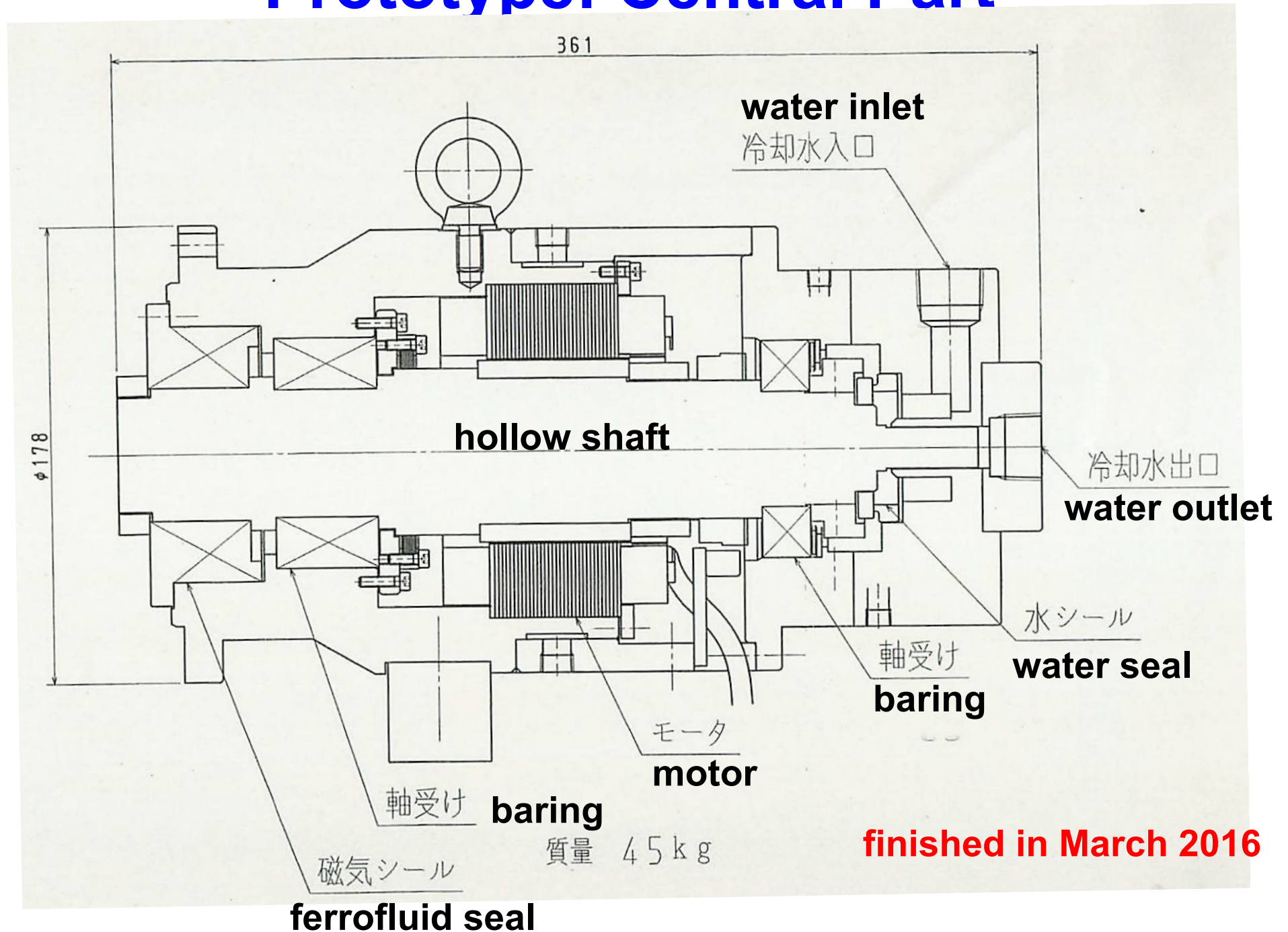


Old plan:
We start making the disk beginning of JPY2016.

But, due to budget situation, we postpone making the disk for 1 year.

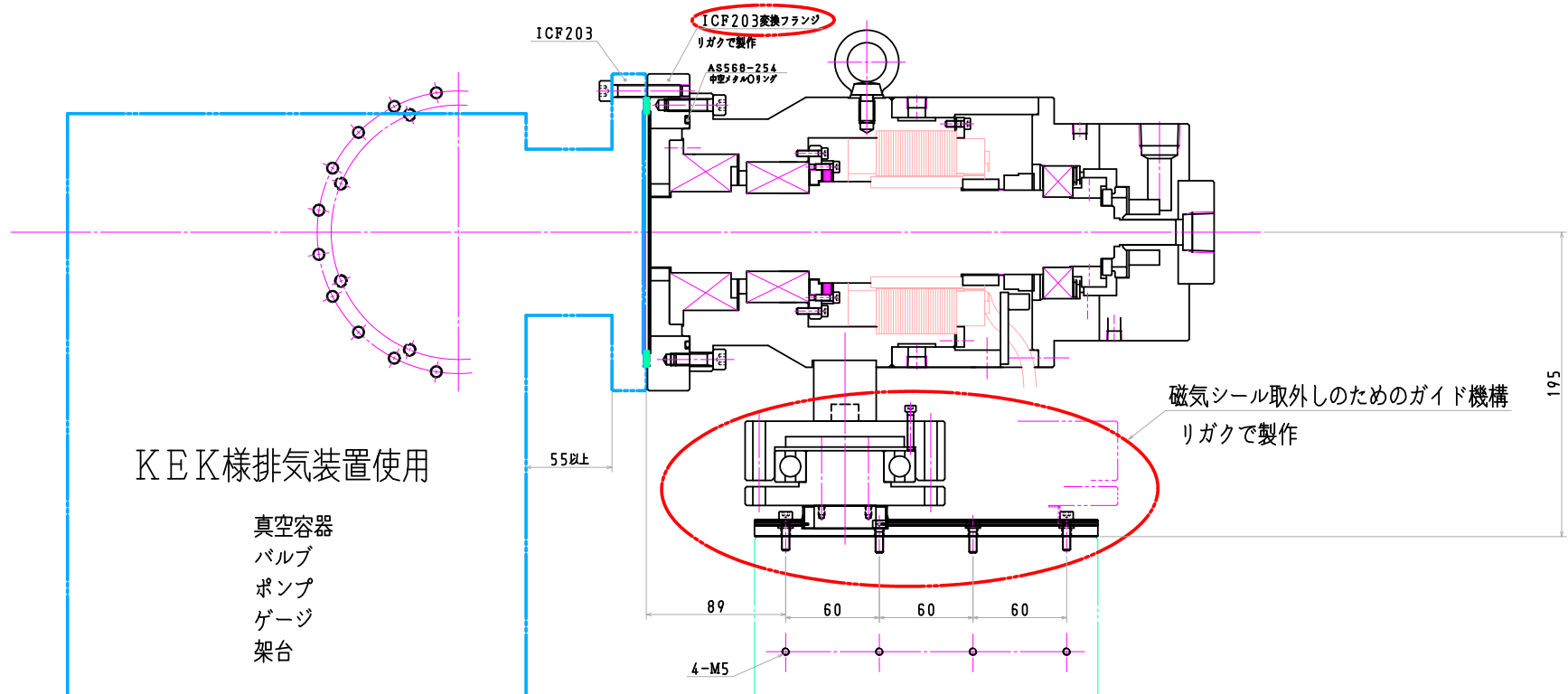
回転ターゲットプロトタイプ概略断面図

Prototype: Central Part



Central Part Prototype Vacuum Test Plan in 2016 June-November

磁気シール実験システム



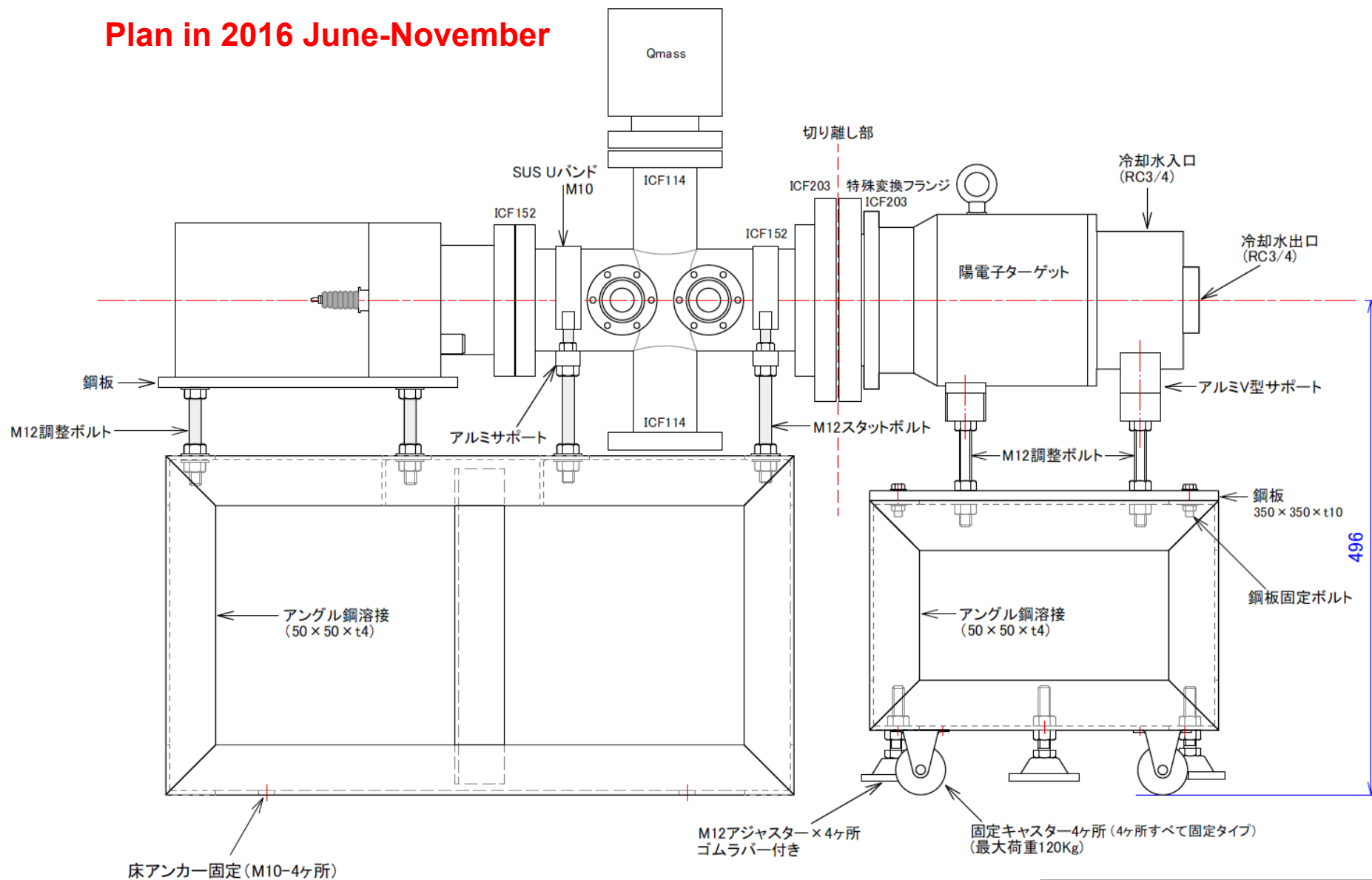
Vacuum Level


Visual Check of ferrofluid after several month of operation

Residual Gas Analyzer

Central Part Prototype Vacuum Test

Plan in 2016 June-November



日付 DATE	2016/7/25	設計 DESIGNED	枝川	図名 TITLE	架台参考図面
尺度 SCALE	1:5	単位 UNIT	mm	品名 NAME	ターゲット真空試験 一式
 株式会社 アシストエンジニアリング ASSIST engineering Ltd.				型式 MODEL	高エネルギー加速器研究機構殿
				図番 DRW No.	K16-050

Summary

Summary

1. Heat and Stress Simulations:

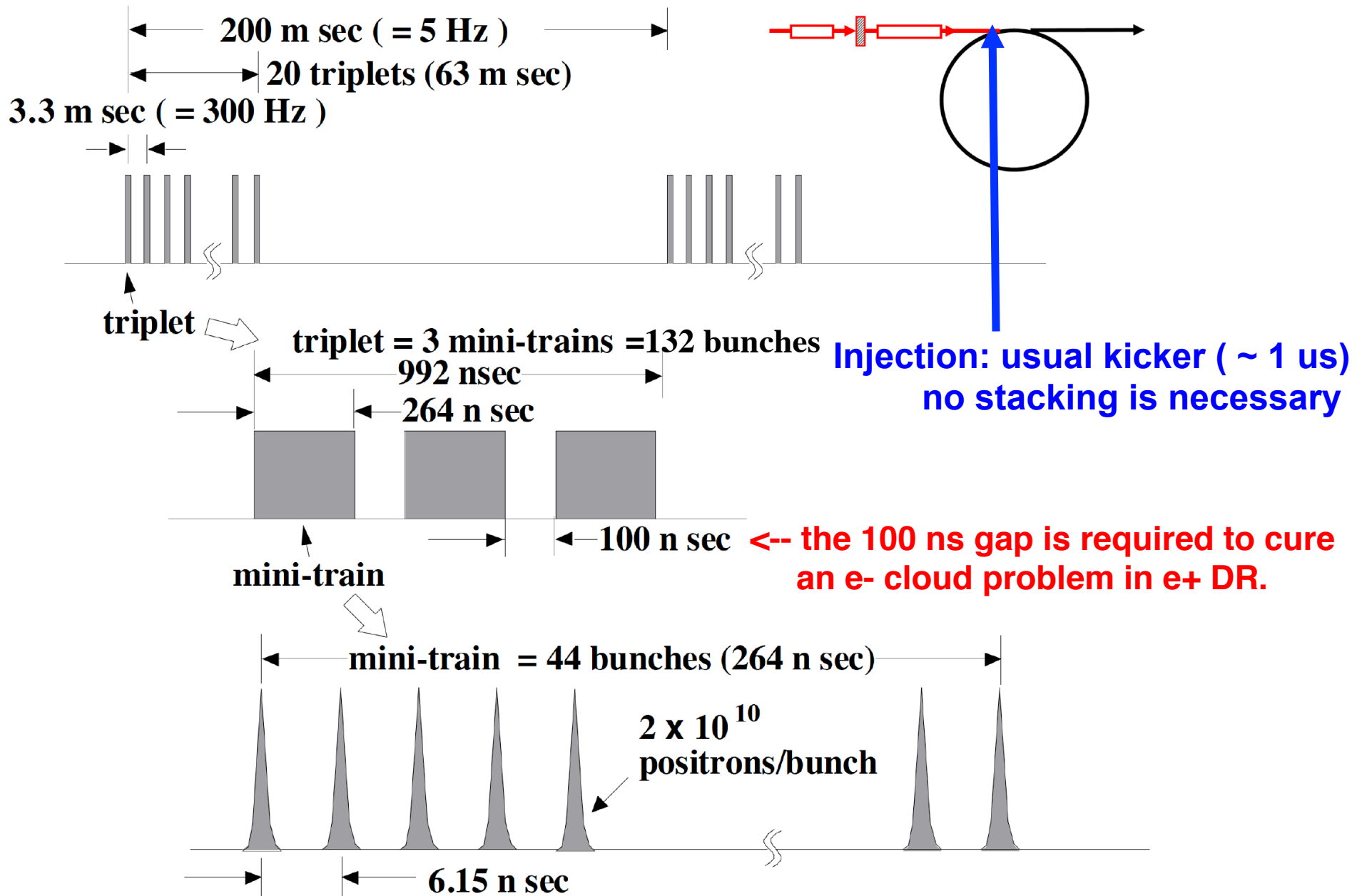
- Max stress of ILC target and SLC target are comparable.
- SLC target survived 3-4 years.
- Comparison of Number of hit / Year.mm
$$N_{ILC} = N_{SLC}/10$$
- We are pursuing better cooling for more safety.
- Possible stress reduction by divided rim?

2. Vacuum Issue and Prototype Target

- **Irradiation test of the whole system** (small off-the-shelf rotation target) was performed. **NO problem** was found.
- Central part of the prototype was finished.
- Disk and large vacuum vessel delay due to budget.
- Central part vacuum test is planed in November 2016.

Backup

Beam before DR



Conventional e+ Source for ILC

Normal Conducting Drive and Booster Linacs in 300 Hz operation

e+ creation

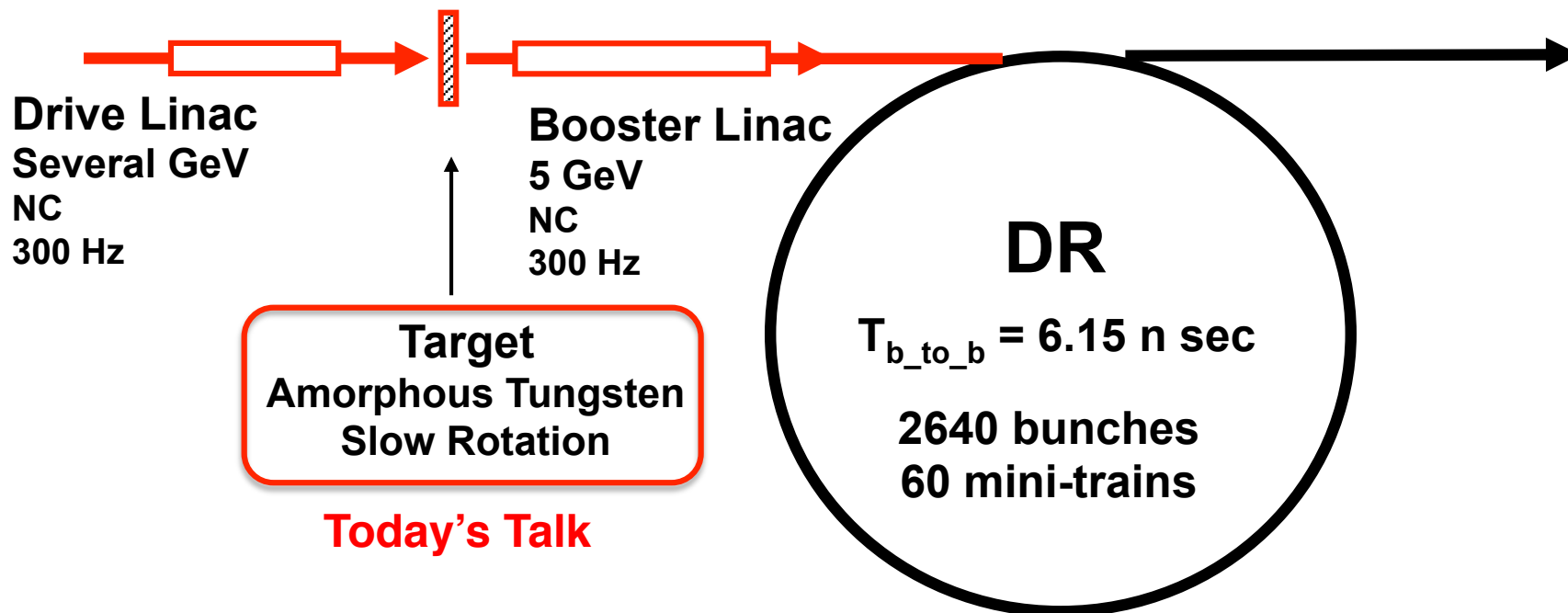
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- $T_{b_to_b} = 369$ n sec



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← Stretching

NIM A672 (2012) 52—56

Thermal Analysis: Target Model and Cooling Condition

FY2014-2015

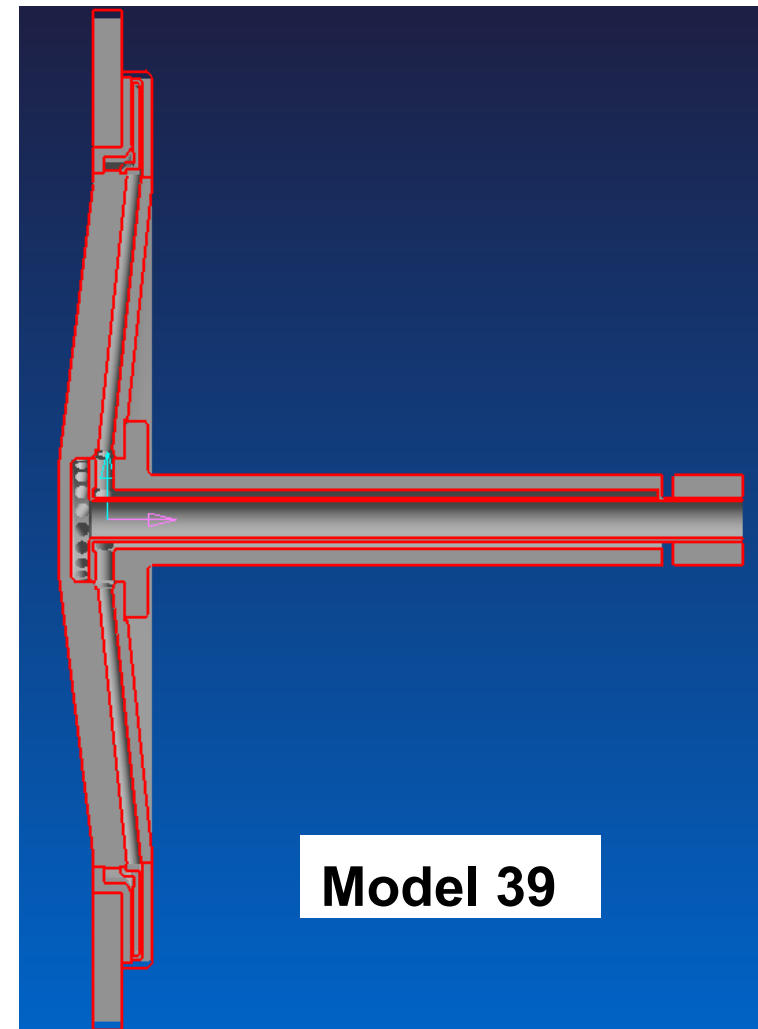
Model : **500 mm diameter** rotation target

Rim ($\phi 500$ - $\phi 366 \times 14$ t) W + Central Cu Disk (water flow inside)

Rotation: 200 - 600rpm

Water temperature at inlet: 25 °C

Software; ANSYS CFX



Points of the prototype

The loads on the vacuum seal and the bearing are determined by the weight and the moment of the target disk. So we will make full size prototype.

**The purpose is vacuum test.
It is not necessary to use W for the disk.
We don't use W for cost saving.**

**Water channels will be unimplemented. It is cost saving.
Target rotation is slow, water circulation is within the past experience of the company. We have no need to demonstrate.**

TEST: Radiation Tolerance **FY2014** More systematic study for CN oil

November 2014

Leading With Innovation



粘度の違いは見られるが、外見に異常なし

Seal against Ar

シール対象：Ar

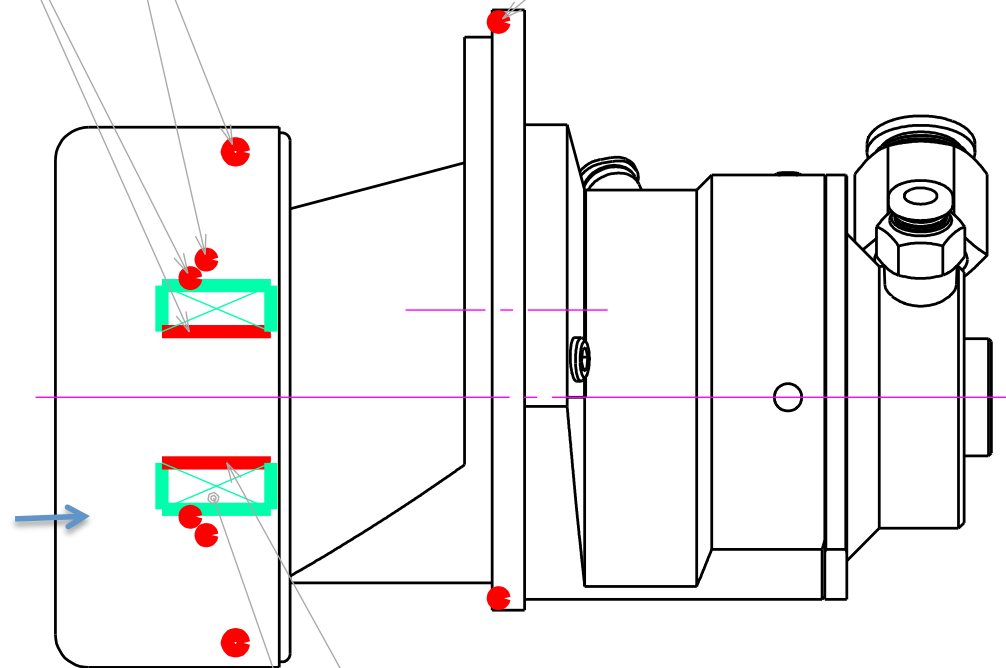
Seal against Water

シール対象：水

Seal against Air

シール対象：空気

Ar-purging →



磁性流体

Ferrofluid seal

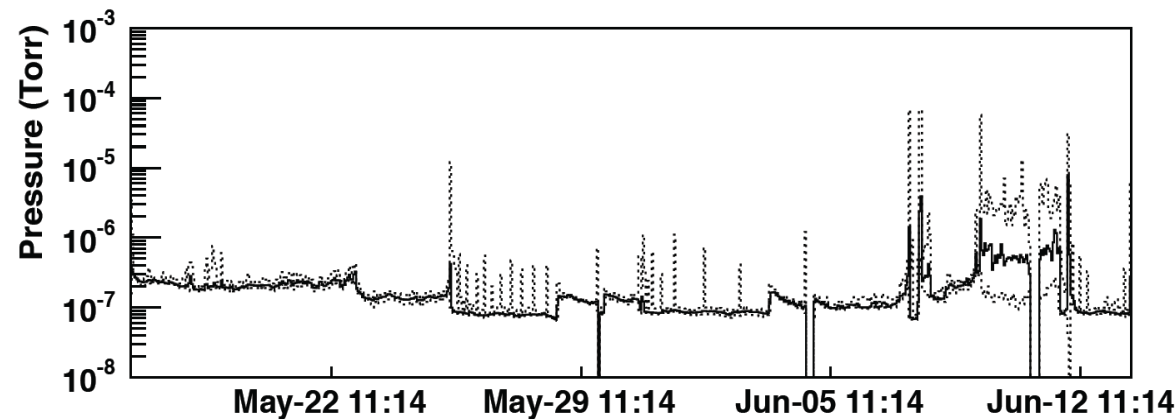
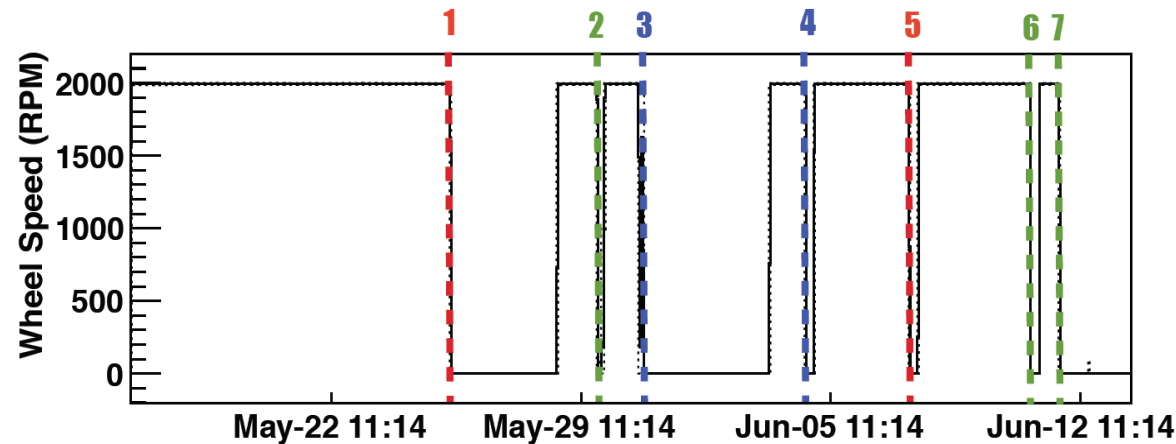
磁気シール

Magnet

その他チャンバー内十数ヶ所にメタルパッキング使用 シール対象：空気

undulator source: Vacuum test of rotation seal

FerroTec Seal #1 ran for 1 month (450 hours up)



Pressure Trip

System Trip

Planned Down

1 - Pressure Spike

2 - DAQ software change

3 - Cooling water flow

4 - Vibration Limit

5 - Pressure Spike

6 - Wheel stopped for pressure test

7 - System down for rework



Lessons Learned

- Ferrofluidic seals are not boring, each one has its own individual personality
 - We would prefer them to be anonymously interchangeable and predictable
- They all have outgassing spikes
 - A differential pumping region just after the seal would be a useful modification
- We are pushing them to speeds at which there is significant heat dissipation
 - Off-the-shelf models do not seem to be well designed for this.
 - Improved cooling design is a must for any future system



Rotation target design study: ongoing with Rigaku

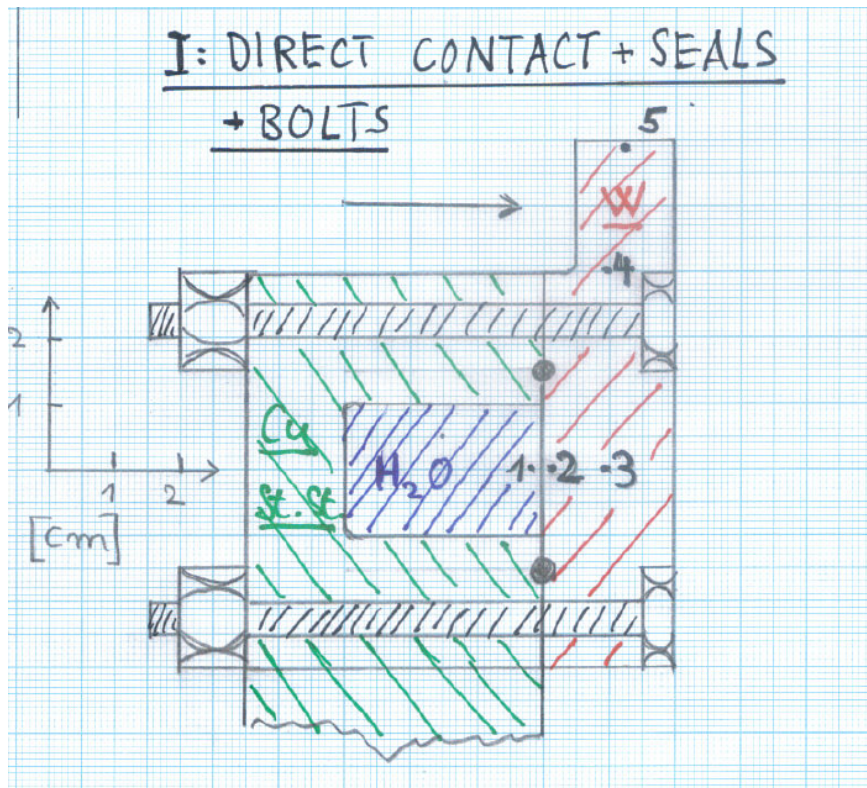
FY2014-2015

Points:

**Diameter, material, shape, rotation speed, cooling,,,
B-filed on the target disk (Hiroshima),
Flux concentrator (IHEP, BINP)**

Peter SIEVERS (CERN)

- I Direct Cooling
- I 直接冷却

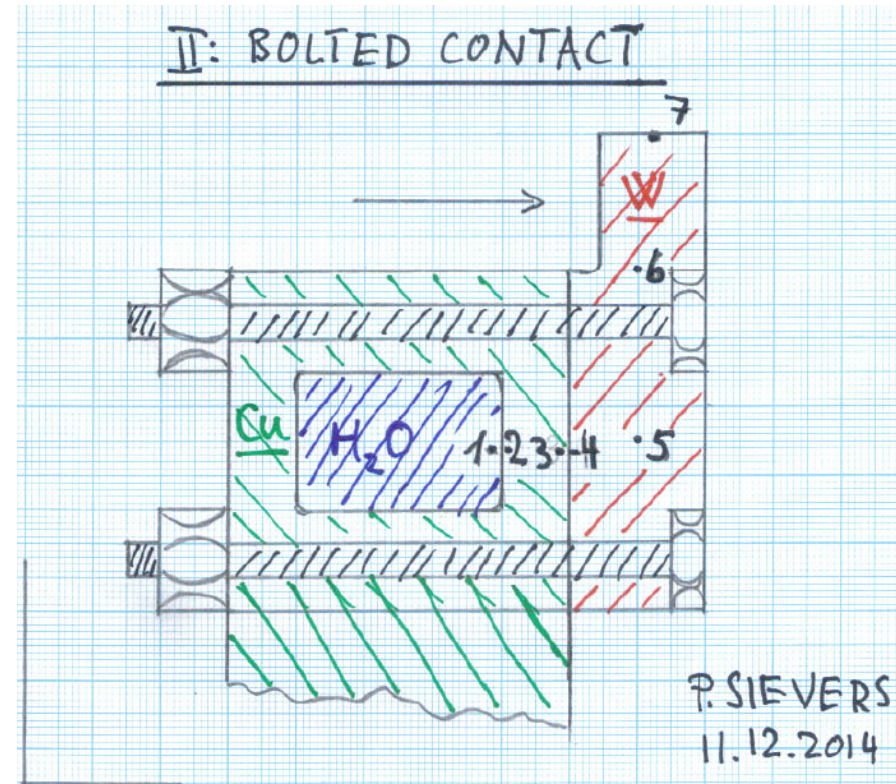


W-Cu joint
metal gaskets
remain UHV leak tight?

Rotation target design study

FY2014

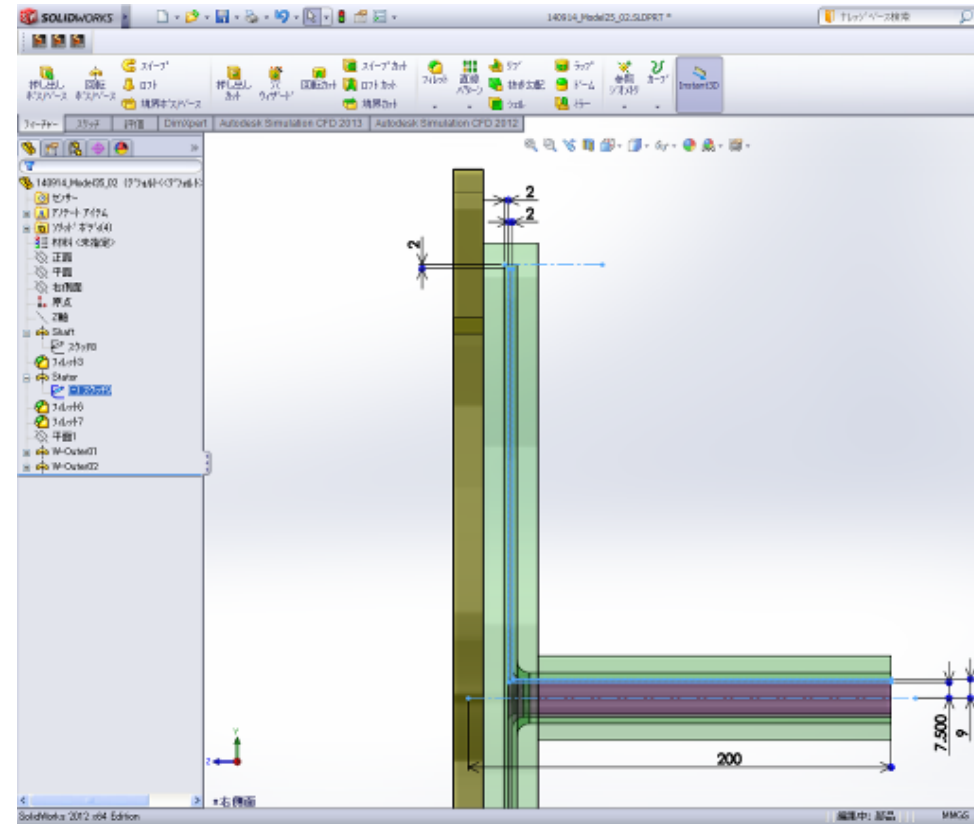
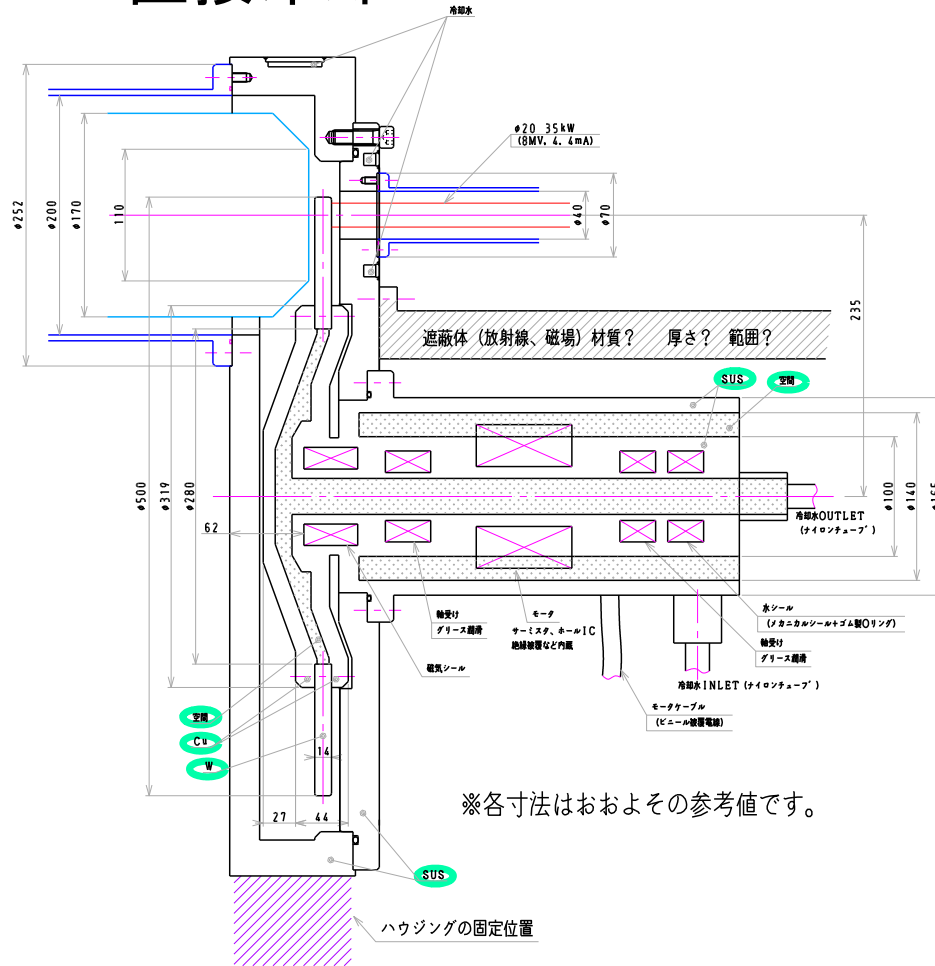
- II Indirect Cooling
- II 間接冷却



"monolithic welded water circuit
entirely of the same material (Cu)"

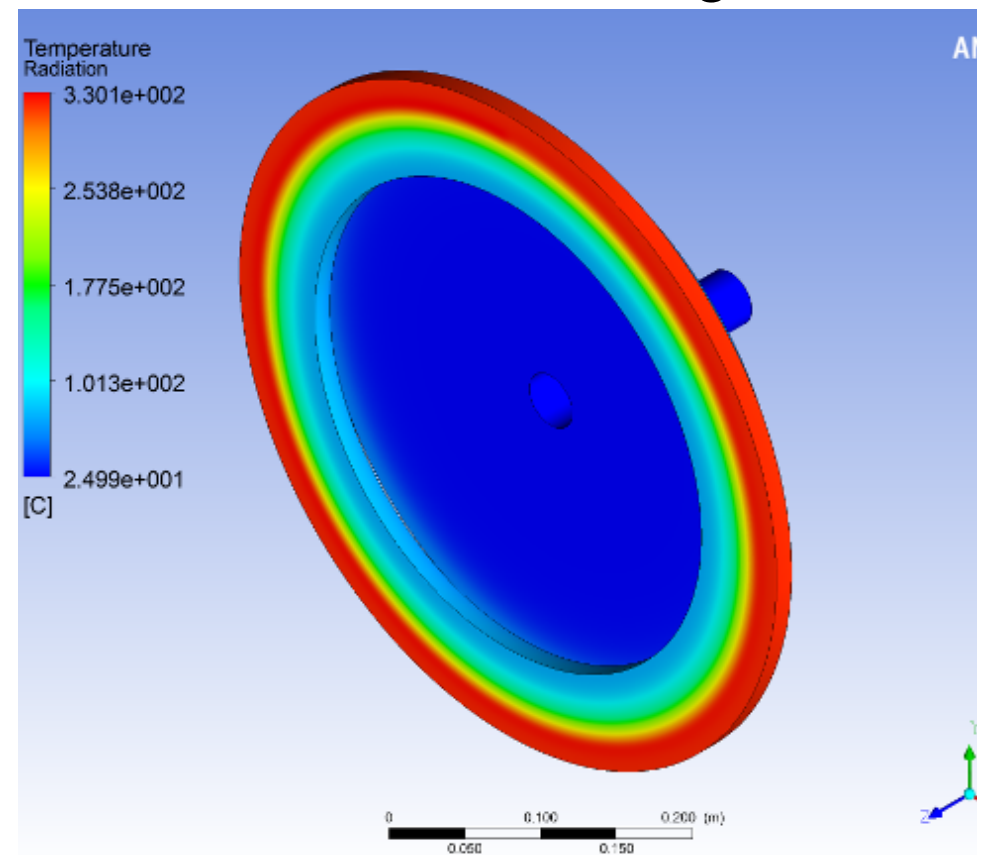
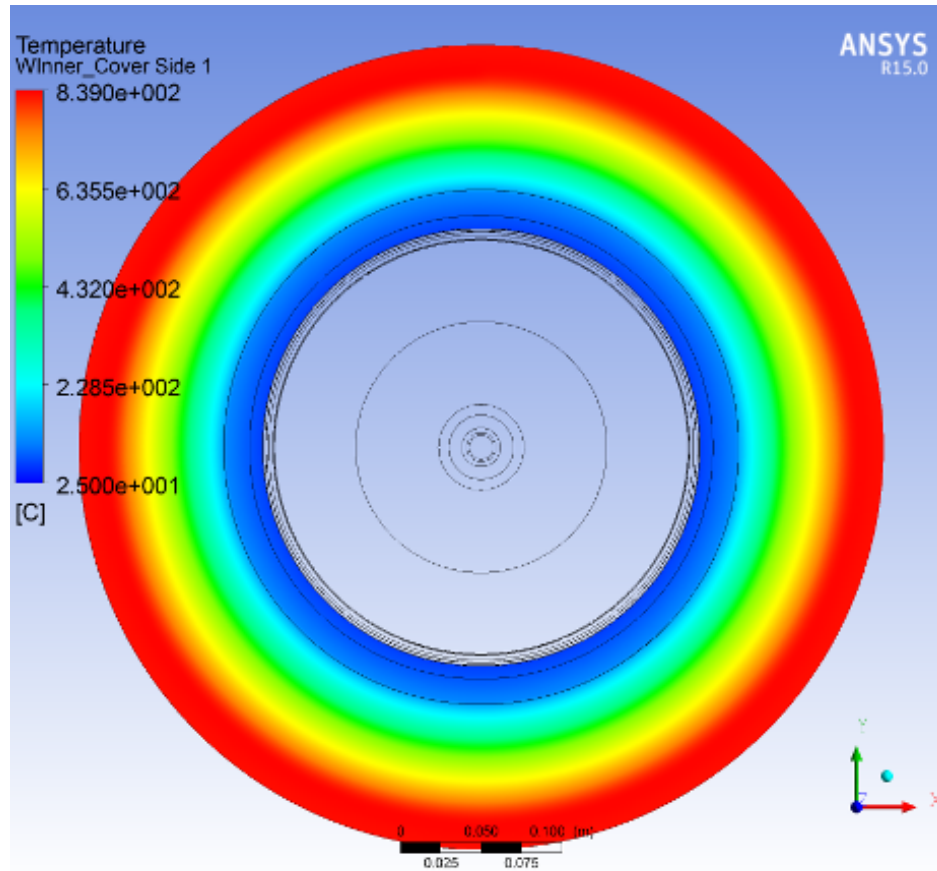
I Direct Cooling
I 直接冷却

II Indirect Cooling
II 間接冷却



I Direct Cooling

II Indirect Cooling



Temperature Distribution

Temperature Distribution

Max. 840°C

Max. 330°C

600rpm
CW Beam

Conclusion: Indirect cooling is better.

TEST: Radiation Tolerance

FY2013: Conclusion

F-oil

Dissociation/degradation occurred at low dose,
0.27 MGy. No hope.

CN-oil

Viscosity increased, but **NO** dissociation/
degradation occurred.

-->

We planed more systematic study.

- Viscosity change as a function of dose.
- Use irradiated fluid in vacuum seal.

**The target R/D
in 2013-2014, and
the first half of 2015.**

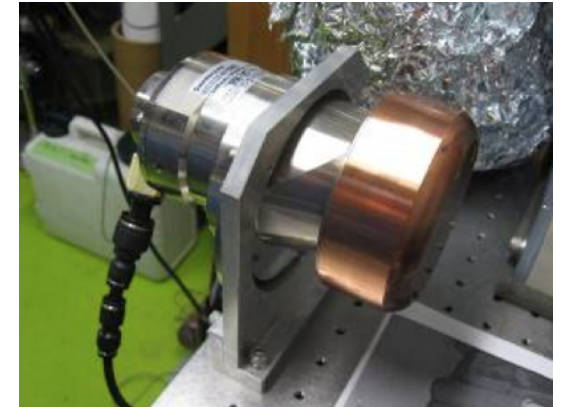
TEST: Vacuum Leak Rate **FY2013**

Conclusion: No problem

Leak Rate Measurement:
various speed, various temperature
no problem (both CN-oil and F-oil)

Leak rate was small enough.

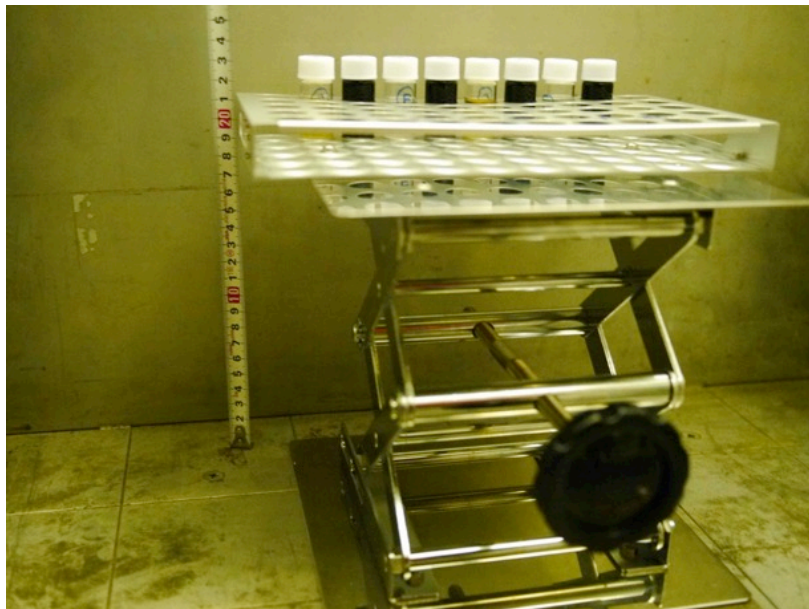
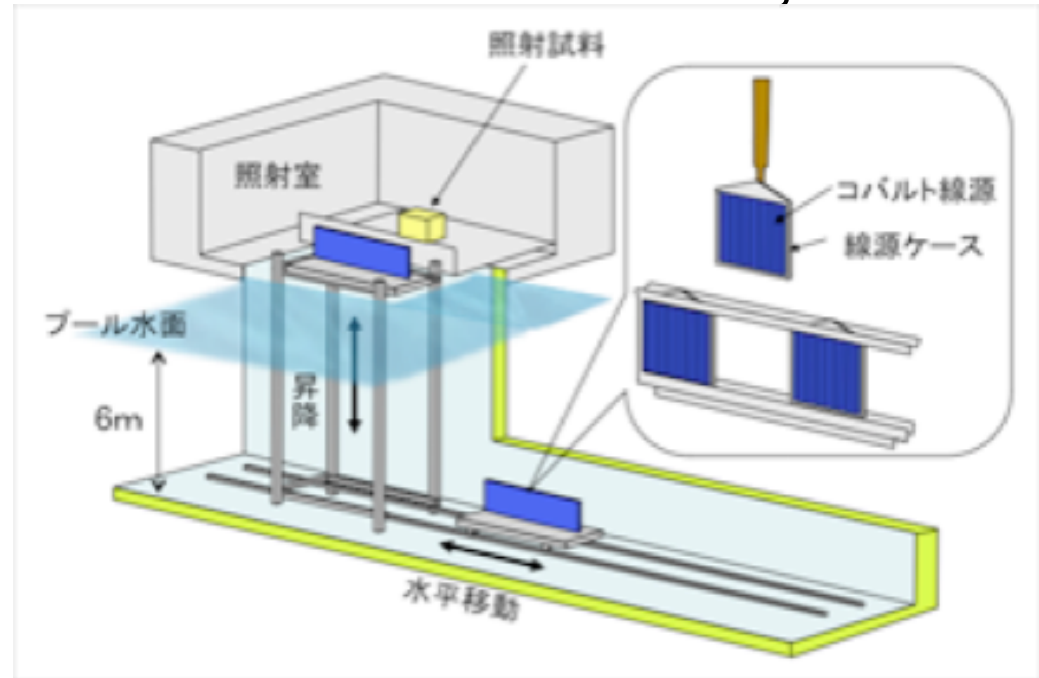
We can get $P < 1 \times 10^{-7}$ Pa, if we put reasonable pumps (several 1000 liters/s) at the upstream of the target.



**Small (d=10 cm)
off-the-shelf
rotation target**

Radiation Tolerance Test **FY2013**

Takasaki Advanced Radiation Research Institute, JAEA



Gamma-ray source: Co 60

1.1×10^4 Gy/h

Photo: Dec/2013

2016年2月4までのシミュレーションのまとめ

(a) 132 bunch (= 一塊 = 回転ターゲットから見た時の1パルス)

が1ヶ所に当たる部分の peak 温度は466 度C

(b) 466 度C の部分のストレスは 530MPa (圧縮)

(c) この状況は安全か？。

500 度C の時の W-Re の fatigue limit は 520 MPa

(Yield Strength は 1300 MPa)

したがって 466 度C で 530 MPa は Fatigue Limit ギリギリの所。

結論

現状設計では Yield strength に対しては十分余裕があるが、Fatigue Limit (多数回の繰り返しを考量した値)を考えるとマージンはゼロ。

Results

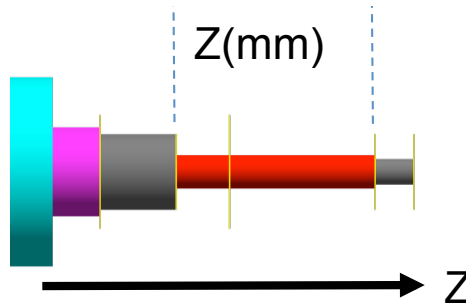
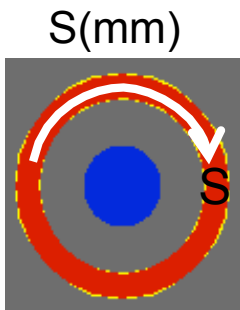
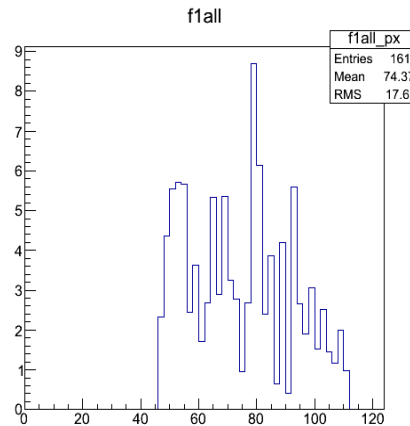
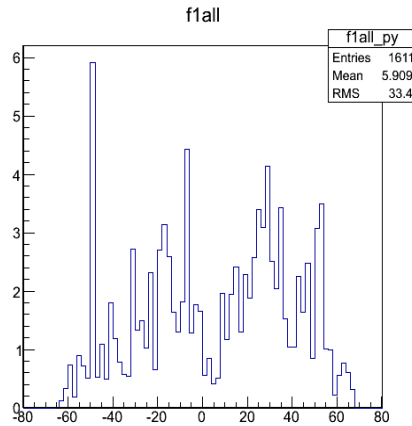
Dose Estimation

FY2014

d = 40 cm with radiation shield

T. Takahashi (Hiroshima)

Energy Depoiti(MeV)/2mm/5x10⁵e-



Peak 1.5MGy/year

(**2630 bunches/pulse**, 5Hz 2e10/bunch 1 year = 10⁷s)

TEST: Radiation Tolerance **FY2014** Takasaki Advanced Radiation Research Institute, JAEA

November 2014



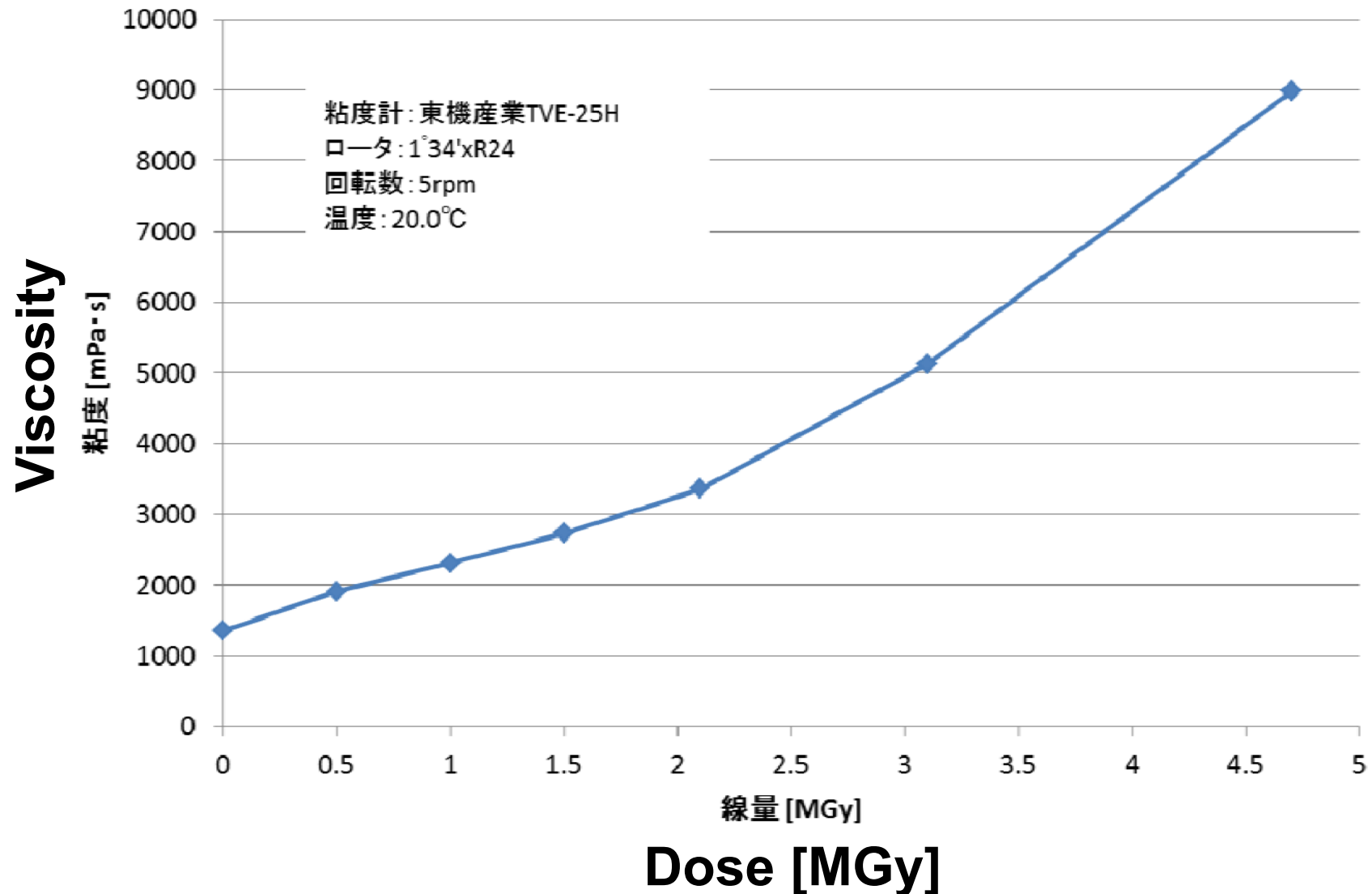
10-Nov-2014

TEST: Radiation Tolerance **FY2014** More systematic study for CN oil

November 2014

Viscosity as a function of dose

放射線量と磁性流体の粘度の関係

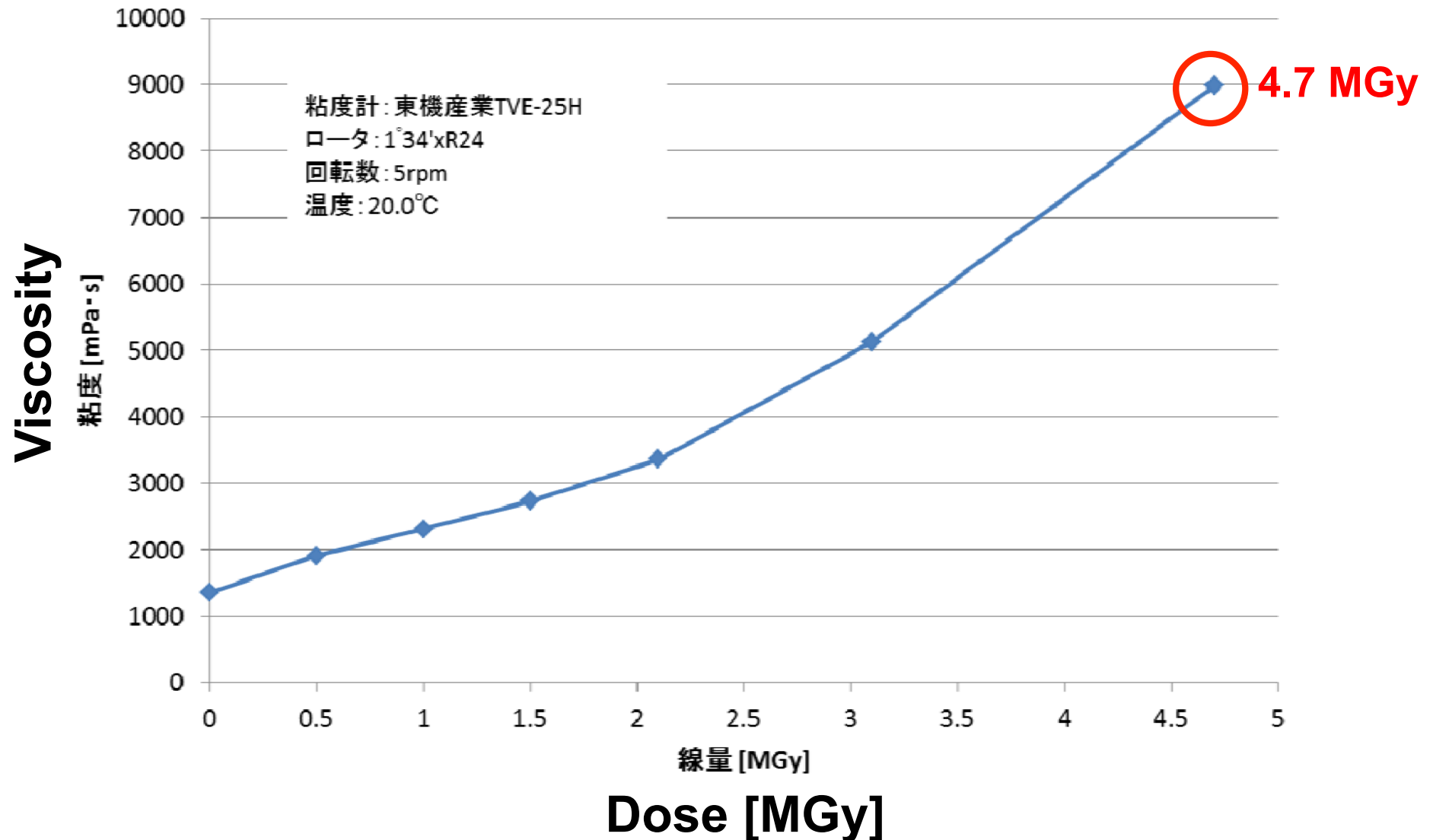


TEST: Radiation Tolerance **FY2014** More systematic study for CN oil

November 2014

Viscosity as a function of dose

放射線量と磁性流体の粘度の関係

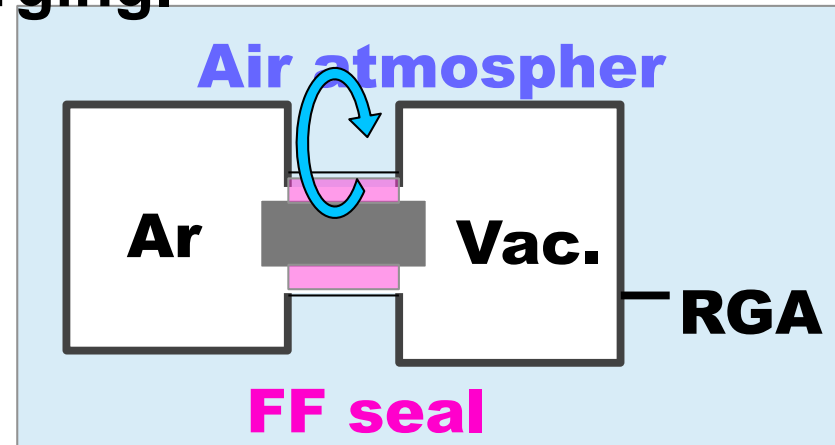


PY2014: Radiation Test:

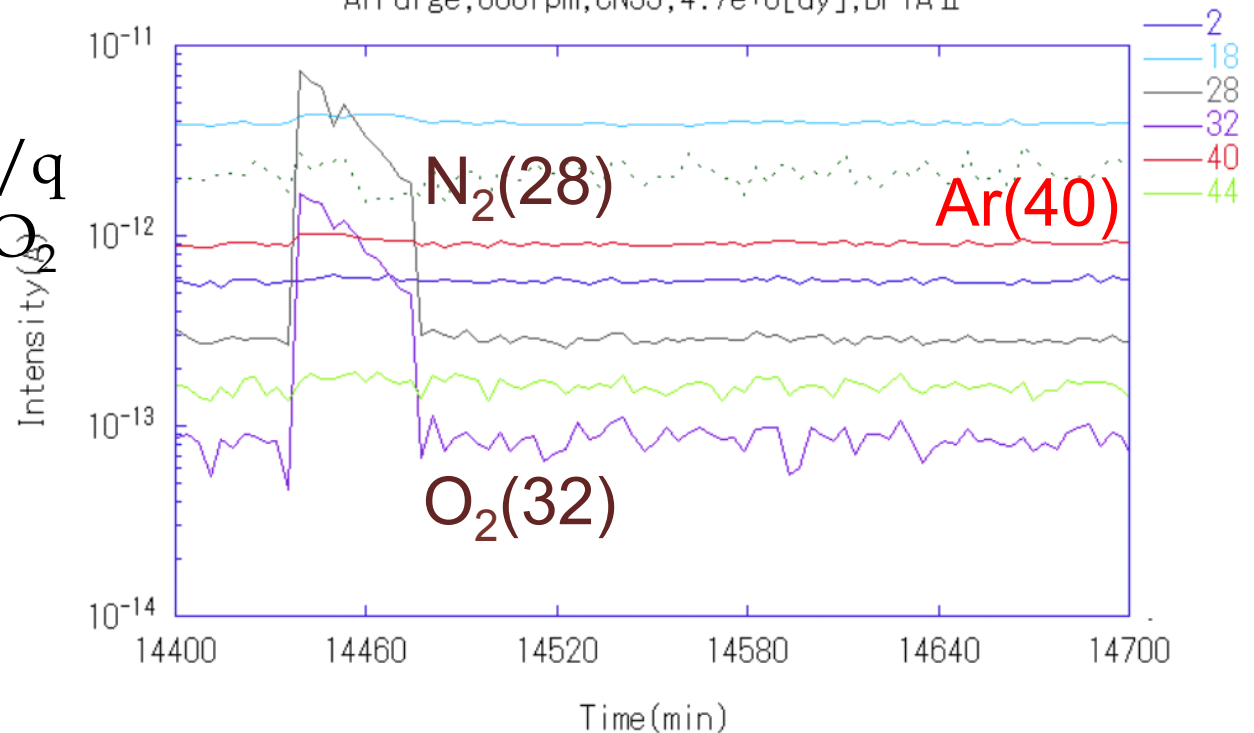
- We used irradiated CN-oil (4.7 MGy) in a small rotation target.
- Made vacuum test after Ar-purging.

Ar purge seal test

- The seal dosed 4.7 MGy (3 ILC year) is examined with Ar purged chamber.
- Rotation : 0-600 rpm.
- **No leak was found.** (m/q = 28 and 32 are N₂ and O₂ from air)

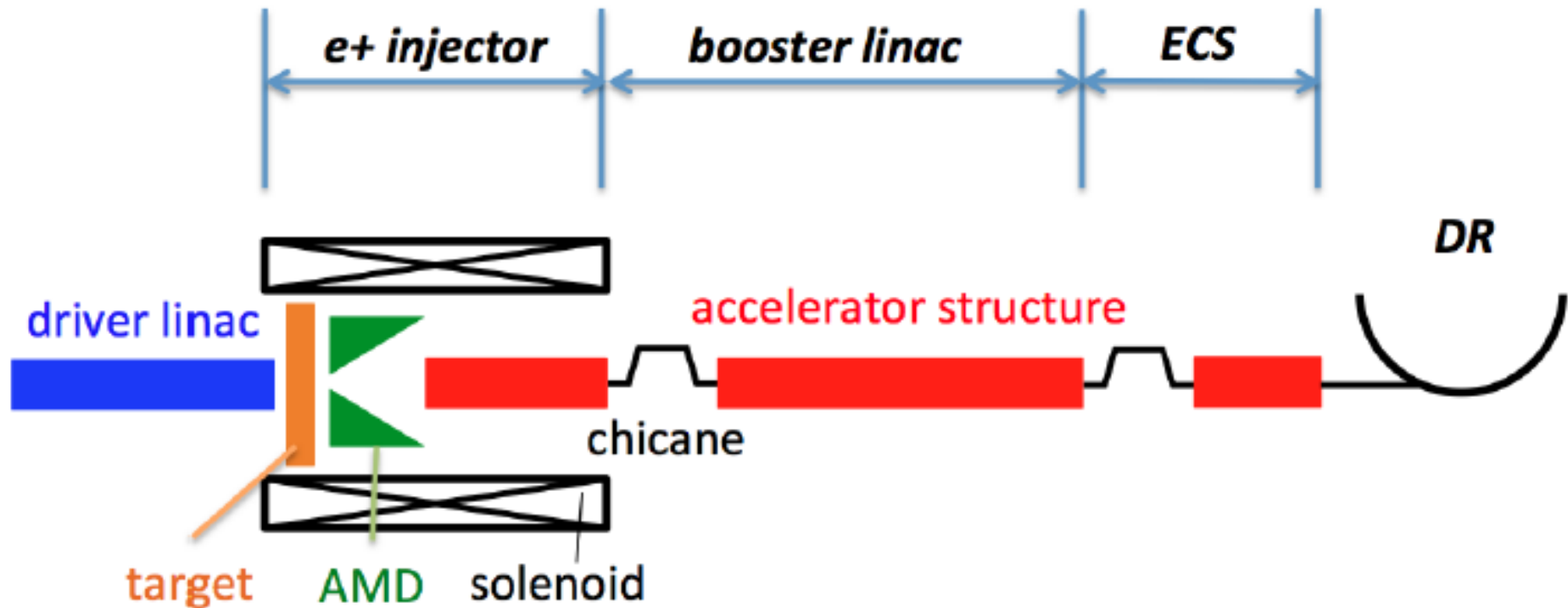


ArPurge,600rpm,CN53,4.7e+6[Gy],DPTA II



AMD is employed as a capture section.
The AMD will be a pulse Flux Concentrator.

Seimiya, Kuriki (Hirosima U.), et al.
Submitted to PTEP



Need to consider the effect of the Flux Concentrator leakage field on the target disk.

FY2014 **Rotation target design study**

The effect of the FC leakage field on the target.

(1) The FC B-field is pulse.

The pulse is fast.

half cycle ~12 micro second (roughly sinusoidal)

Dominant

(2) The target is rotating.

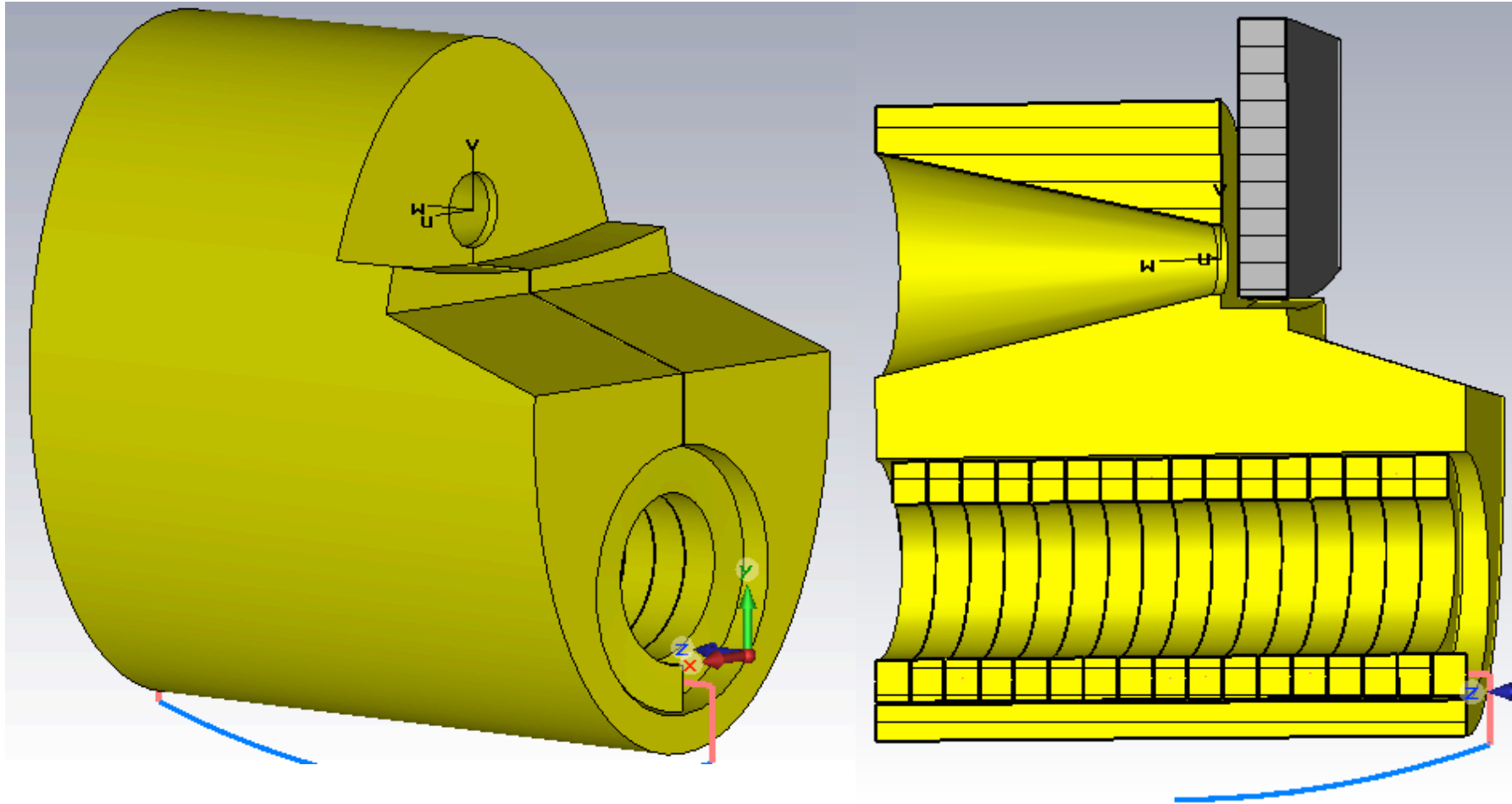
Rotation is slow. ~5 m/s.

Small, Negligible (2)/(1) ~ 1/1000

Pavel Martyshkin (BINP) **FY2015** Rotation target design study

Flux Concentrator (FC) leakage field on the target disk.

Cone diameter is 16 mm (Nose FC)



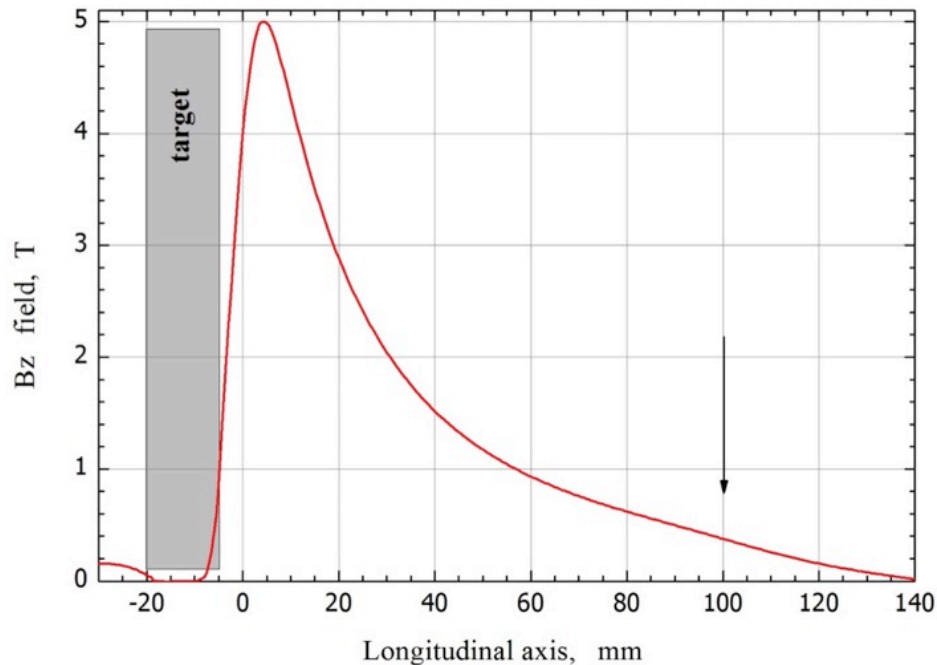
Sun Xianjin (IHEP) also made a study too, based on another design (2014-2015).

Pavel Martyshkin (BINP) FY2015 Rotation target design study

Flux Concentrator (FC) leakage field on the target disk.

Cone diameter is 16 mm (Nose FC)

B = 1 Tesla at Target Disk



Peak current
Peak field
Peak transverse field
Current shape
Current pulse length

Target ohmic loss
FC ohmic loss

Repetition rate 300 pps *

Target losses *

FC losses *

Nose FC type
D 16 mm

25 kA

5 Tesla

50-60 mTesla

half of sine

25 μ s

≈ 10 J/pulse

≈ 140 J/pulse

3.2 kW

41 kW

* When we calculate real average, we need to divide the numbers by three.

Sun Xianjin (IHEP) also made a study too, based on another design.

FY2014-2015

Rotation target design study

The effect of the FC leakage field on the target.

Heating:

1 kW (3.2 kW in 63 msec). It is 1/30 of the heat by beam.

Conclusion: No problem.

Note:

At LCWS2015 (Tsukuba), Omori reported heating is 190kW. It was rough estimate by hand.

Omori reported that we need cure.

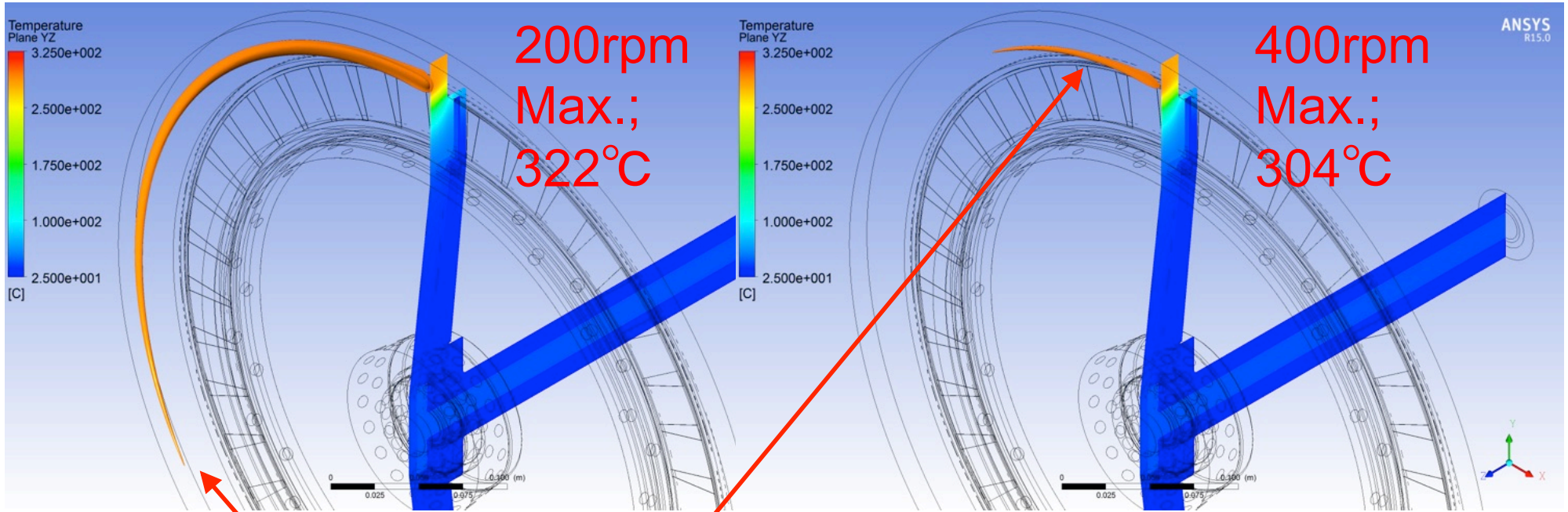
But new conclusion based on detail simulation is NO PROBLEM.

Forces:

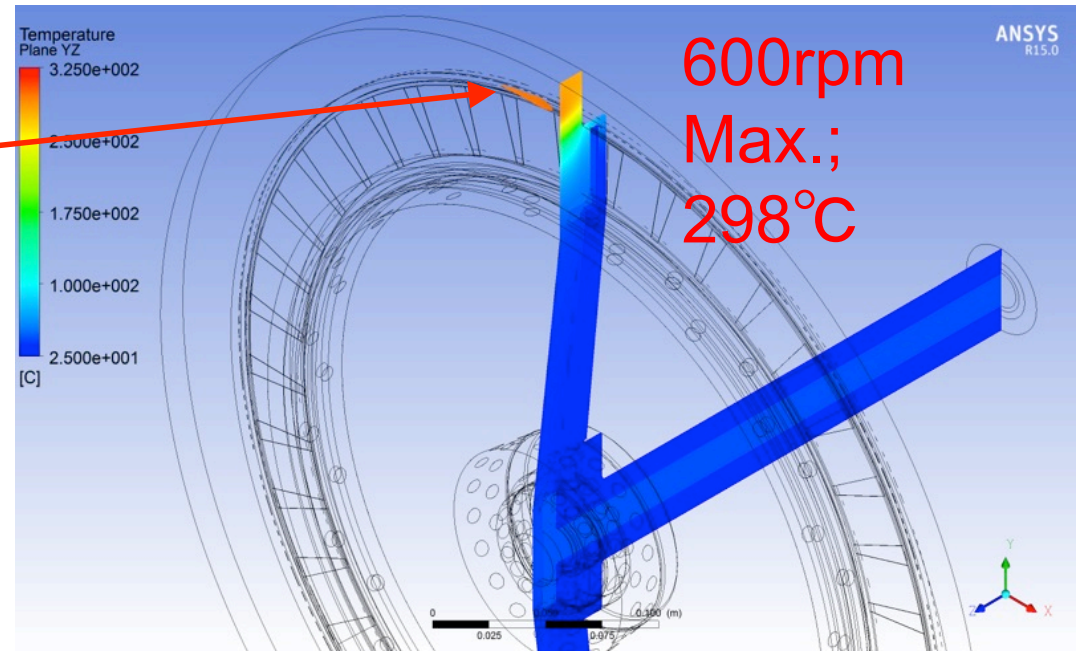
Small in both braking and attractive/repulsive forces.

Conclusion: No problem.

Temperature in various rotation speeds: CW beam analysis

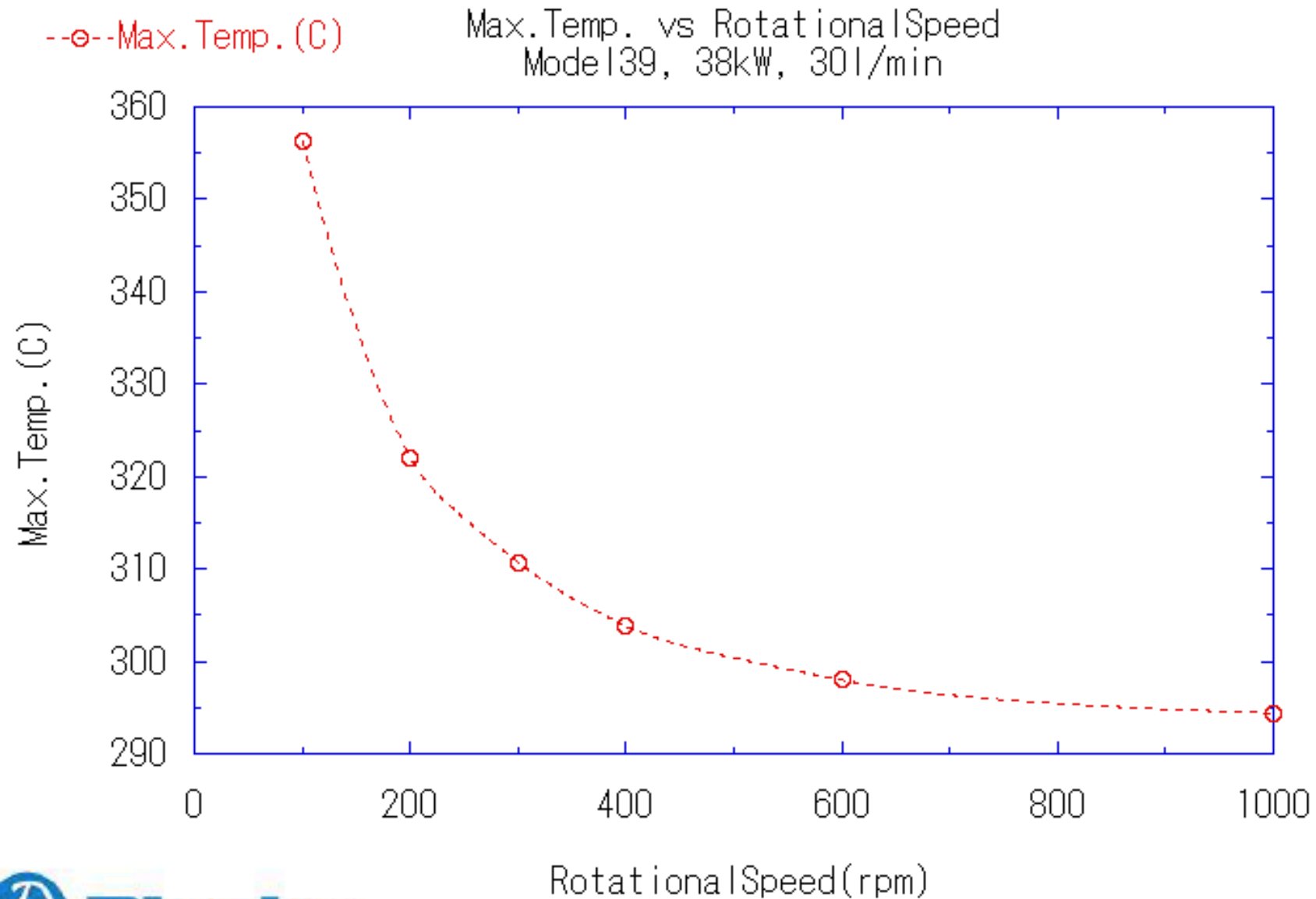


等温度平面;
295°C

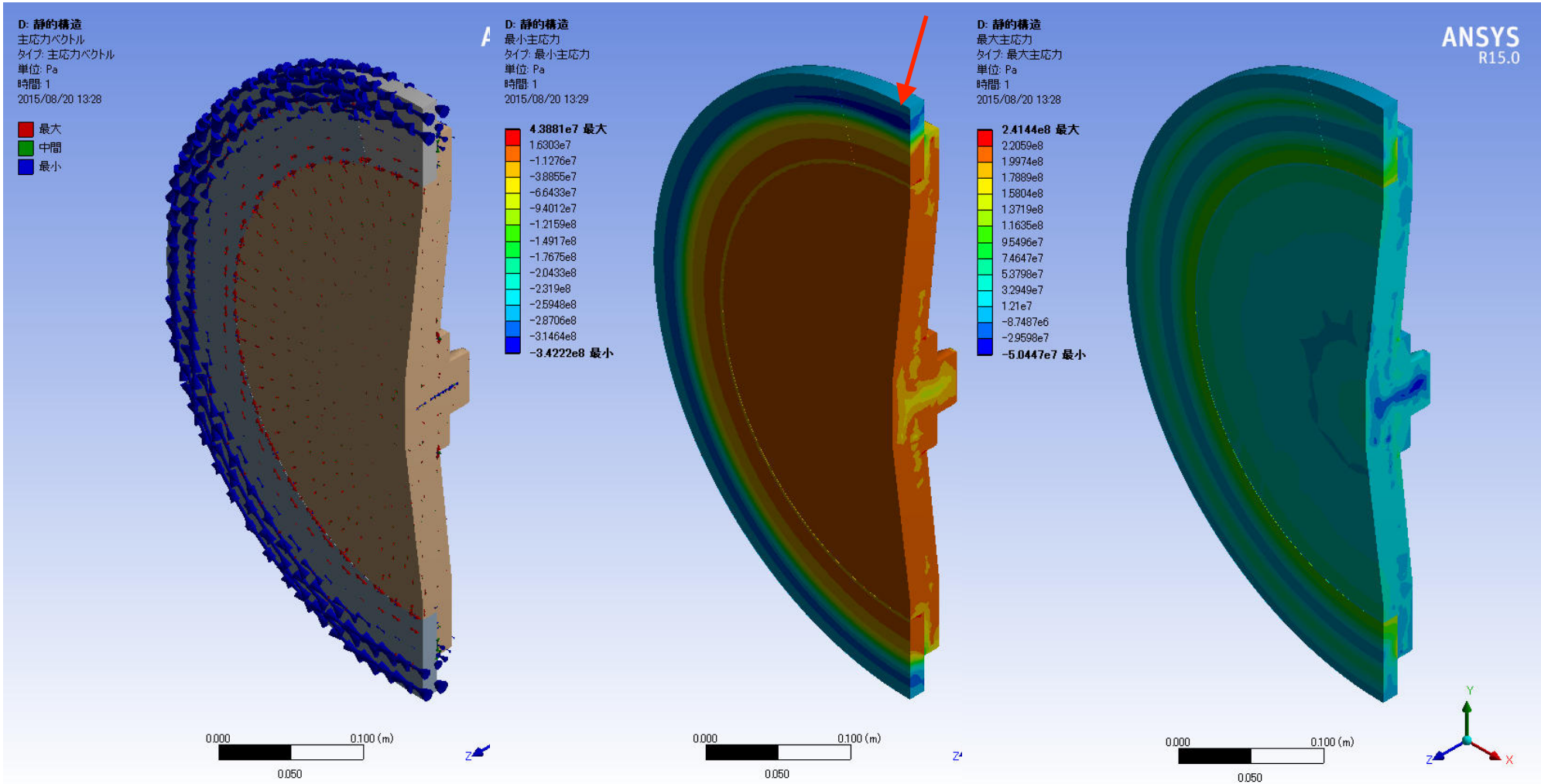


Nb=2600

Temperature in various rotation speeds: **CW beam analysis**



Stress: rotation speed 200 rpm, CW Beam analysis



Direction (arrows)

Min Principal Stress
(Compression)
→ - 3e+8Pa

Max Principal Stress
(Expansion)
→ 2e+8Pa



Nb=2600

高温部の応力を正確に得る為に非定常解析が必要

Thermal Analysis:

We did both **CW beam** analysis (for simplicity) and **pulse beam** analysis (more realistic).

We assume **2600 bunches** in all analysis.

- CW beam analysis

38kW (35kW+3kW^(*)) CW
↑ ↑
beam FC

FY2014-2015

* Note

3 kW is not correct
should be 1 kW

- Pulse beam analysis: **step 1**

114.1 kW(111.1kW+3kW) 63 ms
0 kW (0kW+0kW) 137 ms
↑ ↑
beam FC

FY2015 New
Reported in
Posipol 2015

- Pulse beam analysis: **step 2**

20 trains (pulses) in 63 ms

New²

- Common condition

Cooling water: 30 ℓ /min, T at inlet: 25°C

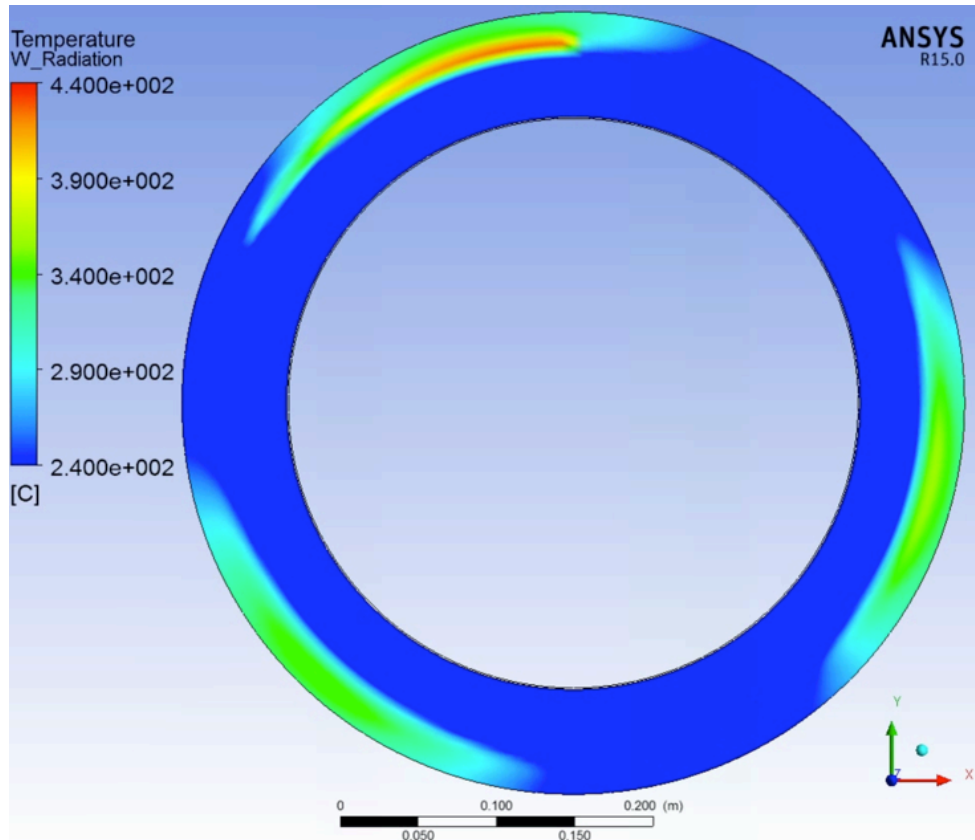


Pulse beam analysis: Comparison of 200 rpm and 220 rpm

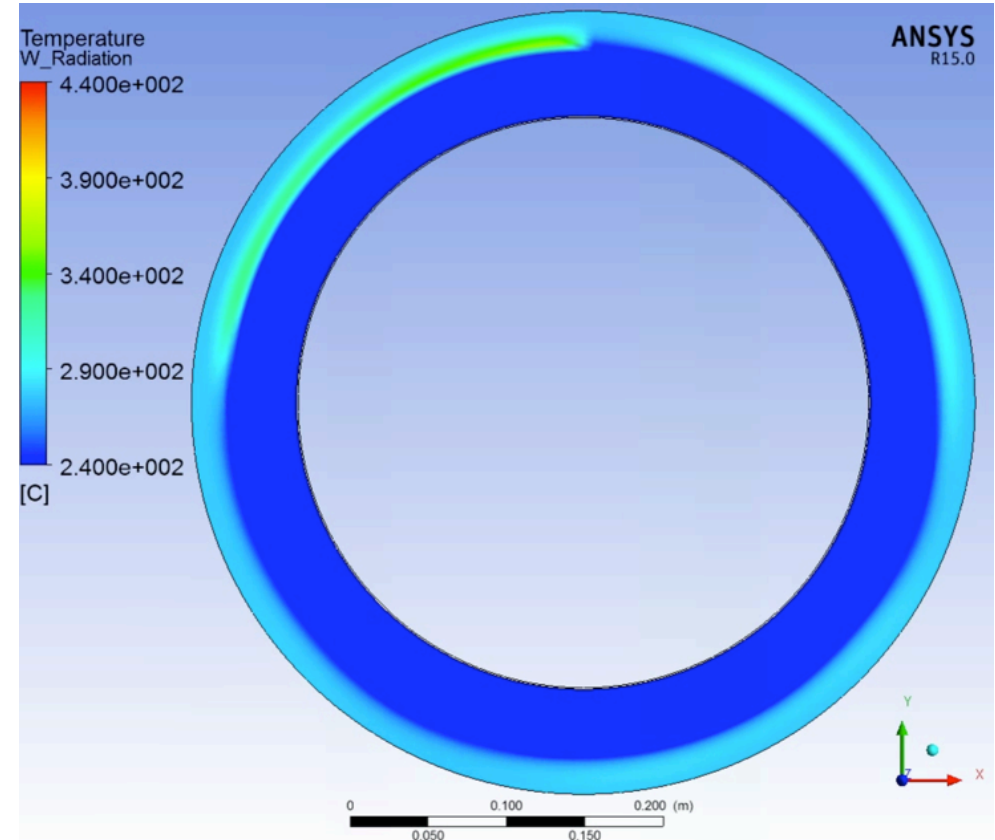
step 1

200 rpm

220 rpm



After reaching steady state
Max Temp = 441 °C



After reaching steady state
Max Temp = 373°C

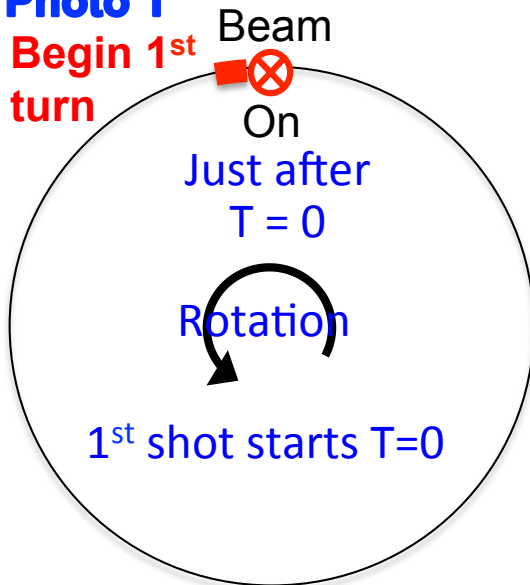
220 rpm is BETTER than 200 rpm.

At 220 rpm: Temperature more UNIFORM and LOWER maximum value.

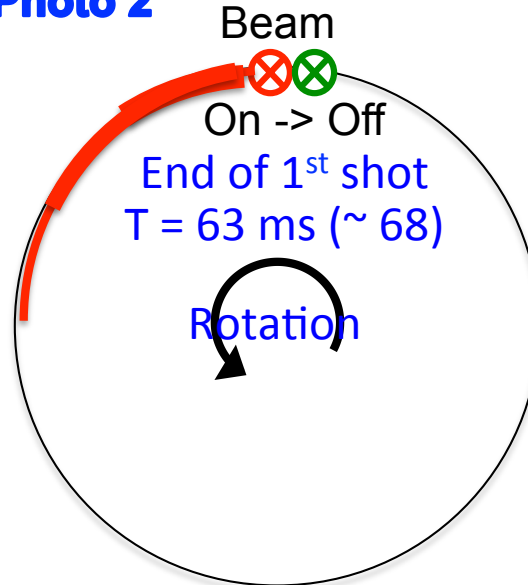
Rotation = 220 rpm : Photos of 1st turn.

Photos = Lab. Frame Views

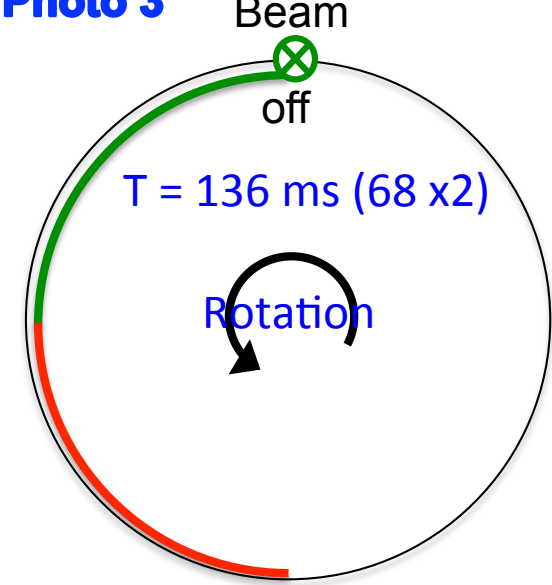
- **Photo 1**
Begin 1st turn



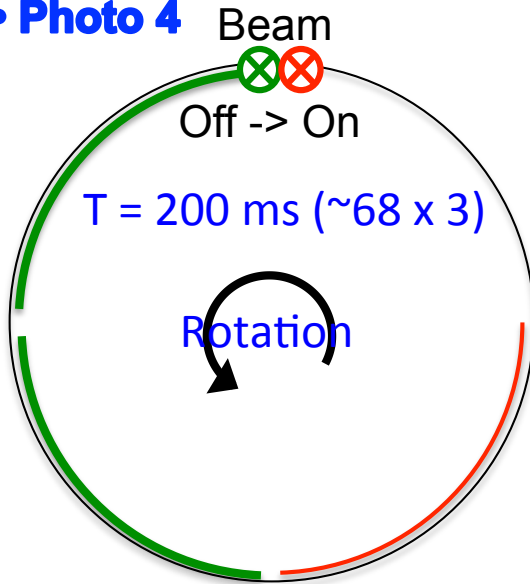
- **Photo 2**



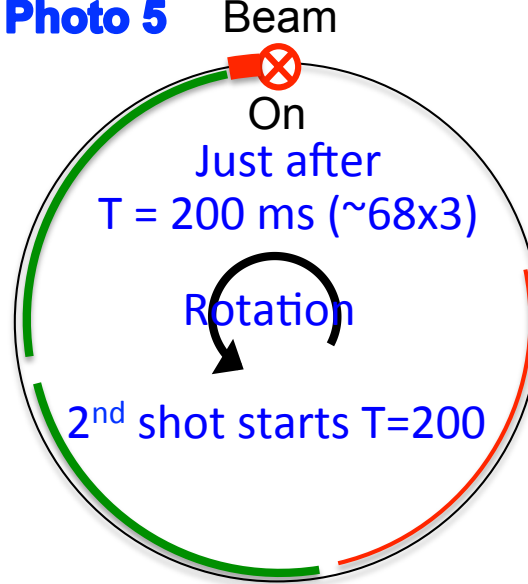
- **Photo 3**



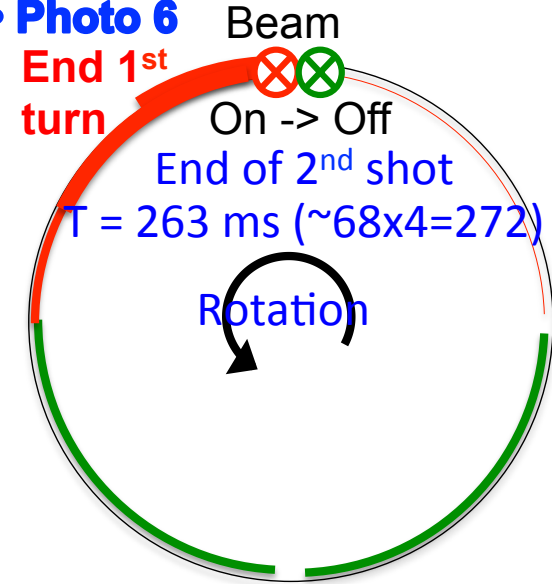
- **Photo 4**



- **Photo 5**



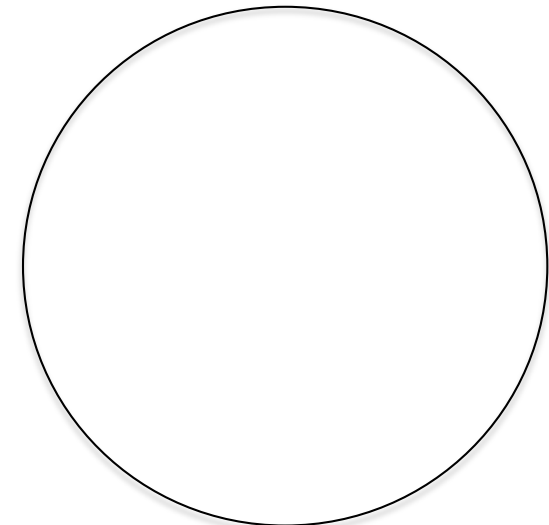
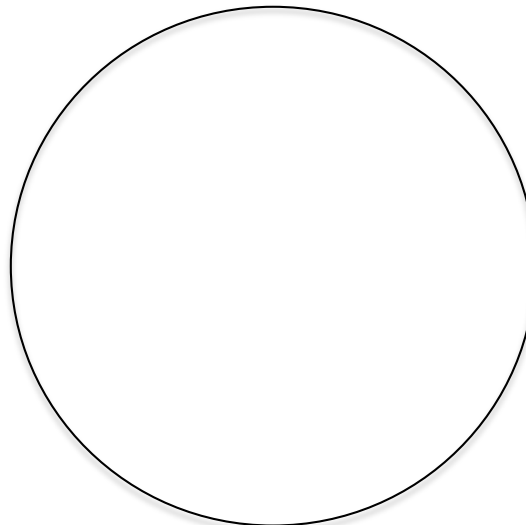
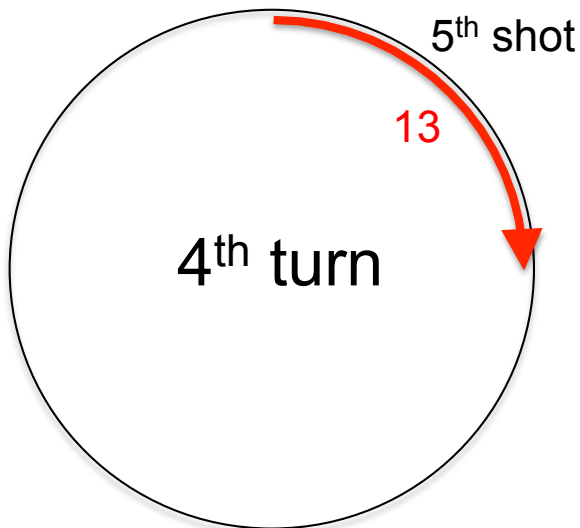
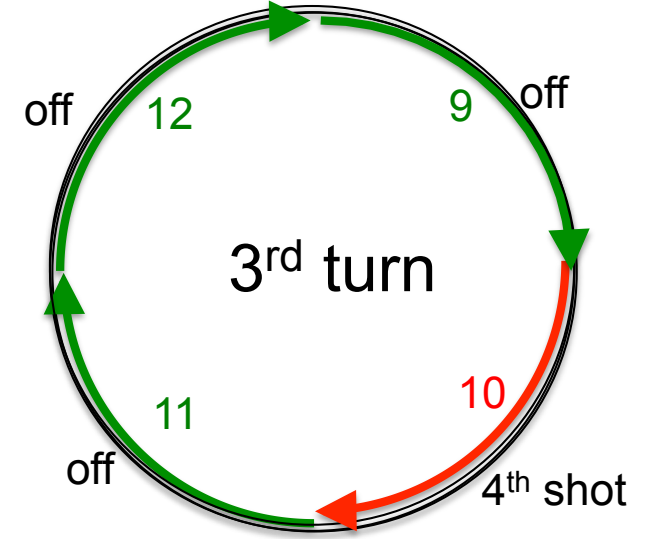
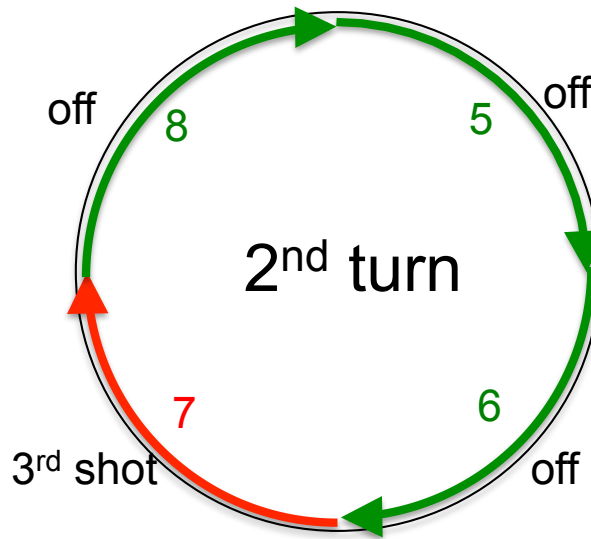
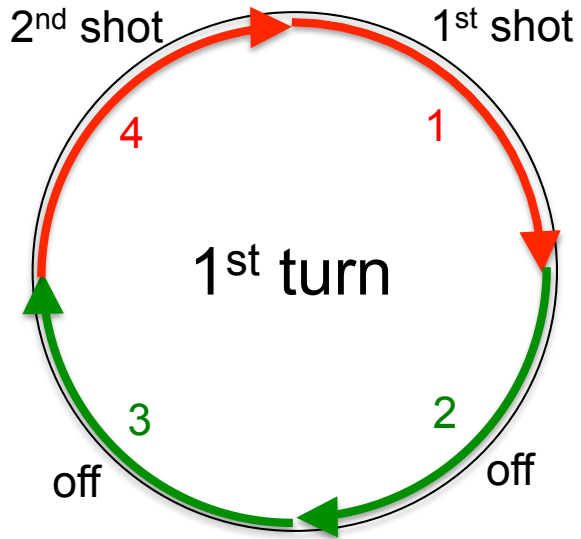
- **Photo 6**



One turn takes 272 m sec. $272 \text{ m sec} / 4 = 68 \text{ ms}$ $68 \text{ ms} \sim 63 \text{ ms}$ (duration of beam on)
 $68 \text{ ms} \times 2 \sim 137 \text{ ms}$ (duration of beam off) $68 \text{ ms} \times 3 = 200 \text{ ms}$ (one cycle of ILC)

Rotation = 220 rpm

Target Rest Frame Views



One turn takes about 272 m sec.

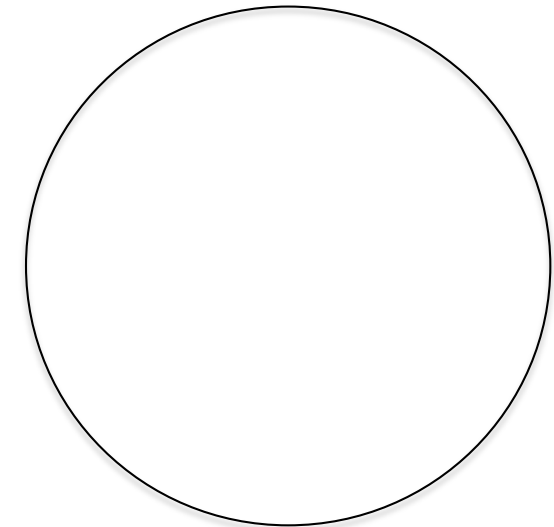
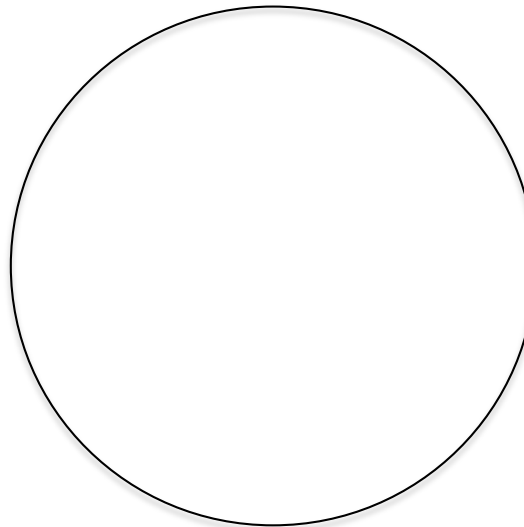
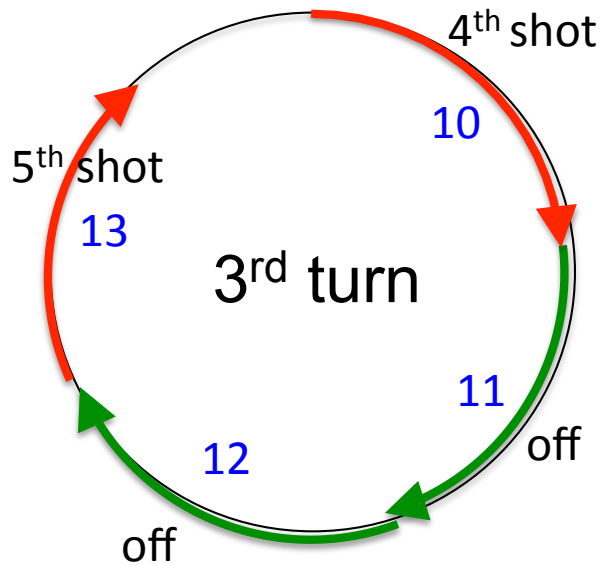
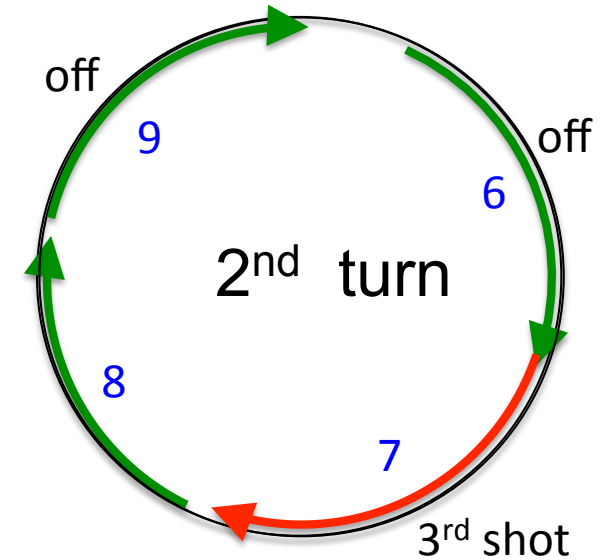
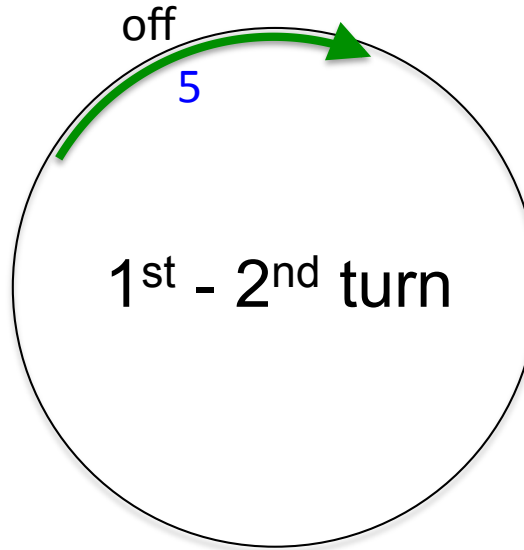
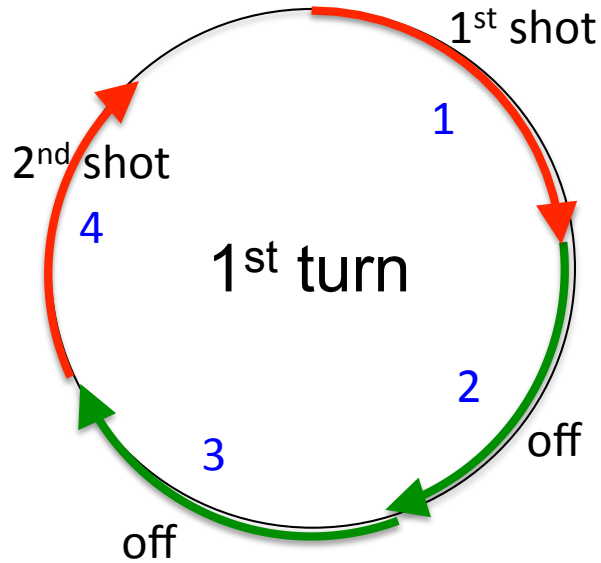
Each Red number (1, 4, 7, 10, 13) corresponds 63 m sec.

Each Green number (2,3, 5,6, 8,9, 11,12) corresponds 68.5 m sec.

63ms + 68.5ms + 68.5ms = 200ms

Rotation = 200 rpm

Target Rest Frame Views



One turn takes about 272 m sec.

Each Red number (1, 4, 7, 10, 13) corresponds 63 m sec.

Each Green number (2,3, 5,6, 8,9, 11,12) corresponds 68.5 m sec.

63ms + 68.5ms + 68.5ms = 200ms

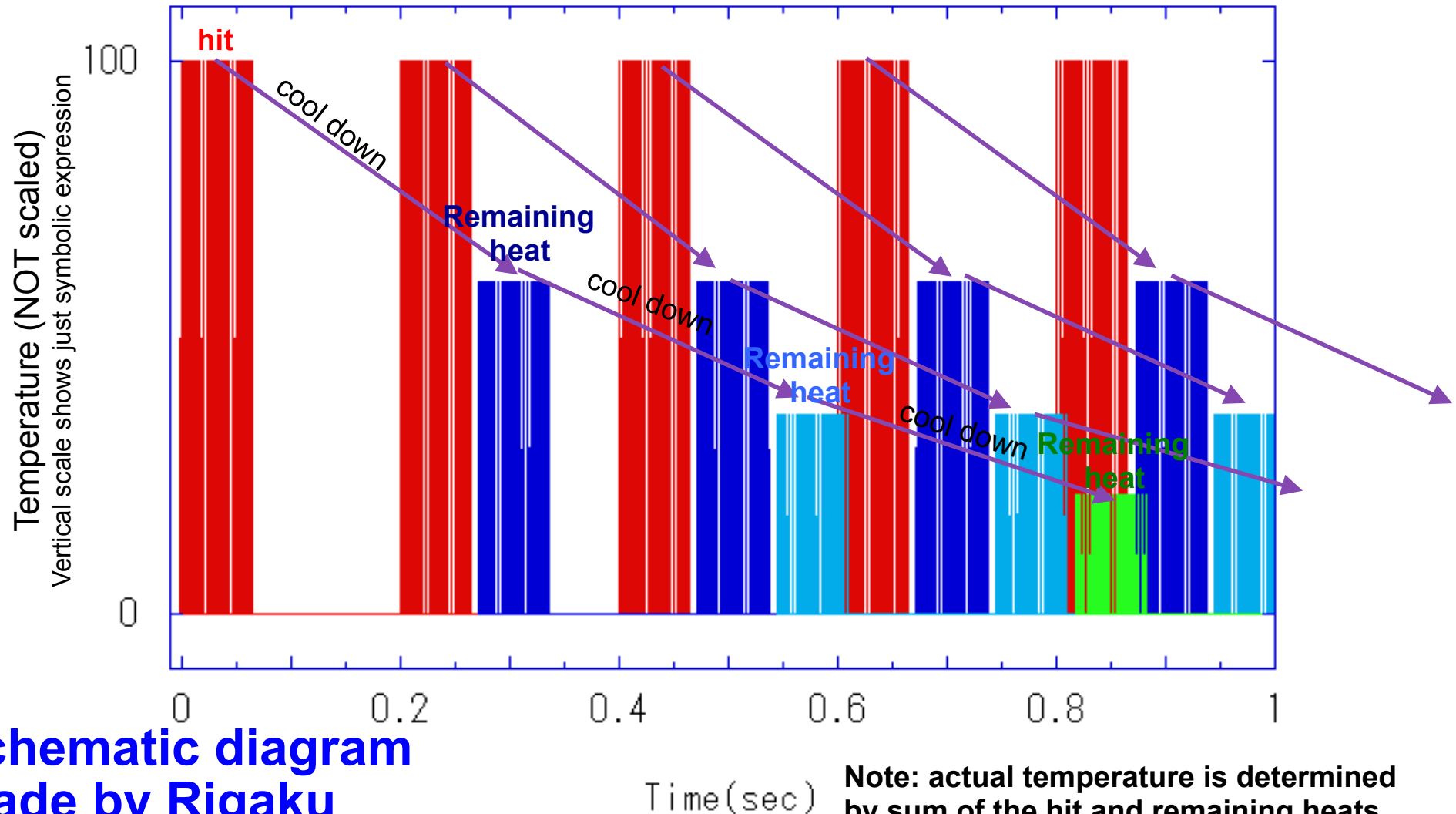
Pulse Beam Diagram

Rotation speed = **220rpm**

hit = 111 kW in 63 ms

Schematic diagram of the first 1 sec.

- 1st
- 2nd
- 3rd
- 4th



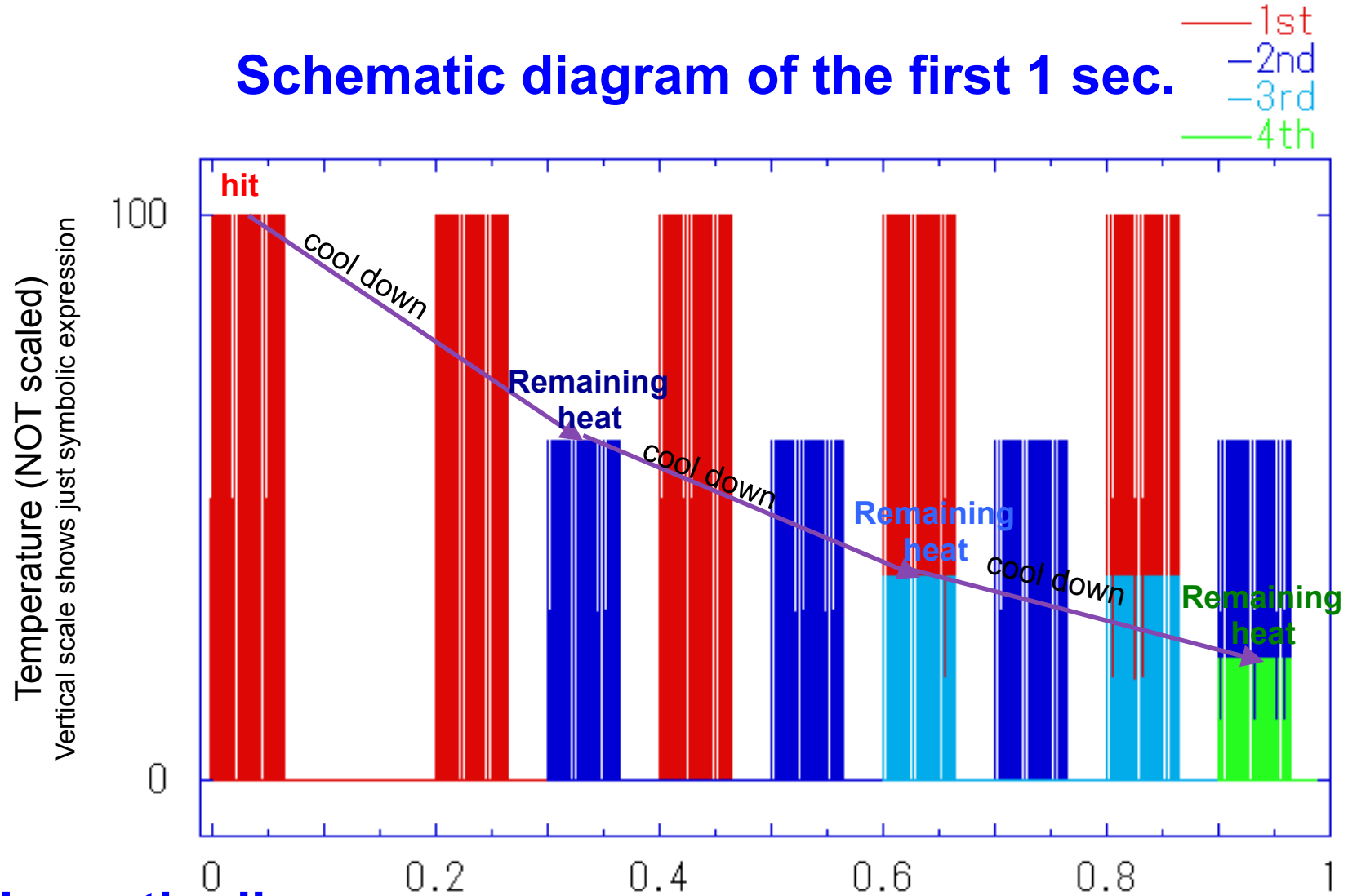
Schematic diagram
made by Rigaku

Pulse Beam Diagram

Rotation speed = **200rpm**

hit = 111 kW in 63 ms

Schematic diagram of the first 1 sec.



**Schematic diagram
made by Rigaku**

Note: actual temperature is determined by sum of the hit and remaining heats.

解釈(これは安全か?)

SLCのターゲットの実績と比べてみる

SLCのターゲットの Max ストレスは約 500 MPa (by Freidrich さん)→ ILC とほぼ同じ

SLAC 自身による解析 (SLAC-PUB-9437) では Max ストレス 560 MPa→ ILC とほぼ同じ

SLCのターゲットは数年の間、壊れずに動いた

解釈(これは安全か?)

SLCのターゲットの実績と比べてみる: 続き 年間の hit 数を比べる

シャワーによるエネルギー密度 (Max) SLCがおおよそ 29 J/g(1バンチ),
ILCのパラメーターは 132 バンチが事実上一ヶ所にあたり、その合計で、約27J/g

パルスあたりのエネルギー密度はほぼ同じと考えていい。(この場合 SLC は1バンチが1パルス、ILC は 132 バンチを纏めて1パルスとしている) これは、Max ストレスが SLC と ILC でほぼ同じであることとコンシステント。

この場合は 入射ビームエネルギーや、ビーム半径の因子は、この数値に繰り込まれているので、パルス数での比が妥当な計算。

ビーム半径の因子はすでに織り込まれていることから、単位面積あたりのパルス数ではなく、単位周長あたりのパルス数を比較する

ビームが落ちる周長の比較

SLCでは 180mm
ILCでは 1500mm

の領域(長さ)がビームを受け入れる。

解釈(これは安全か?)

SLCのターゲットの実績と比べてみる: 年間の hit 数を比べる (続き)

パルス数をこれで除したものが、年間あたりの周長あたりのパルス数。

SLC $120 \times 3600 \times 24 \times 365 / 180 = 2.1 \text{ e}+7 \text{ pulse/year.mm}$

ILC $2600/132 \times 5 \times 3600 \times 24 \times 365 / 1500 = 2.1 \text{ e}+6 \text{ pulse/year.mm}$

(SLC は1バンチが1パルス、ILC は 132 バンチを纏めて1パルスとしている)

年間 hit 数では ILC は SLCとくらべて 10 倍らくと考えられる。

注意:

これはかなり荒っぽい計算

**Summary of the R/D
in Past 2.5 Years:
FY2013-mid.FY2015**

FY2013: Leak Rate measurement

We took leak rate data by using a small (d=10cm) rotation target off the shelf.

Conclusion: Leak Rate is small enough.

FY2013-2014: Radiation Test:

We made radiation test of ferrofluid at Takasaki Lab.

Conclusion:

F-oil: No hope.

CN-oil: No problem up to 4.7 MGy (about 3 ILC years).

FY2014-2015: Target Design Study.

We made design study with the company, Rigaku.

Study included both mechanical design and thermal stress analysis.

We now have a nearly final mechanical design.

Thermal stress study is ongoing.

Pulse Beam Analysis

step 2:

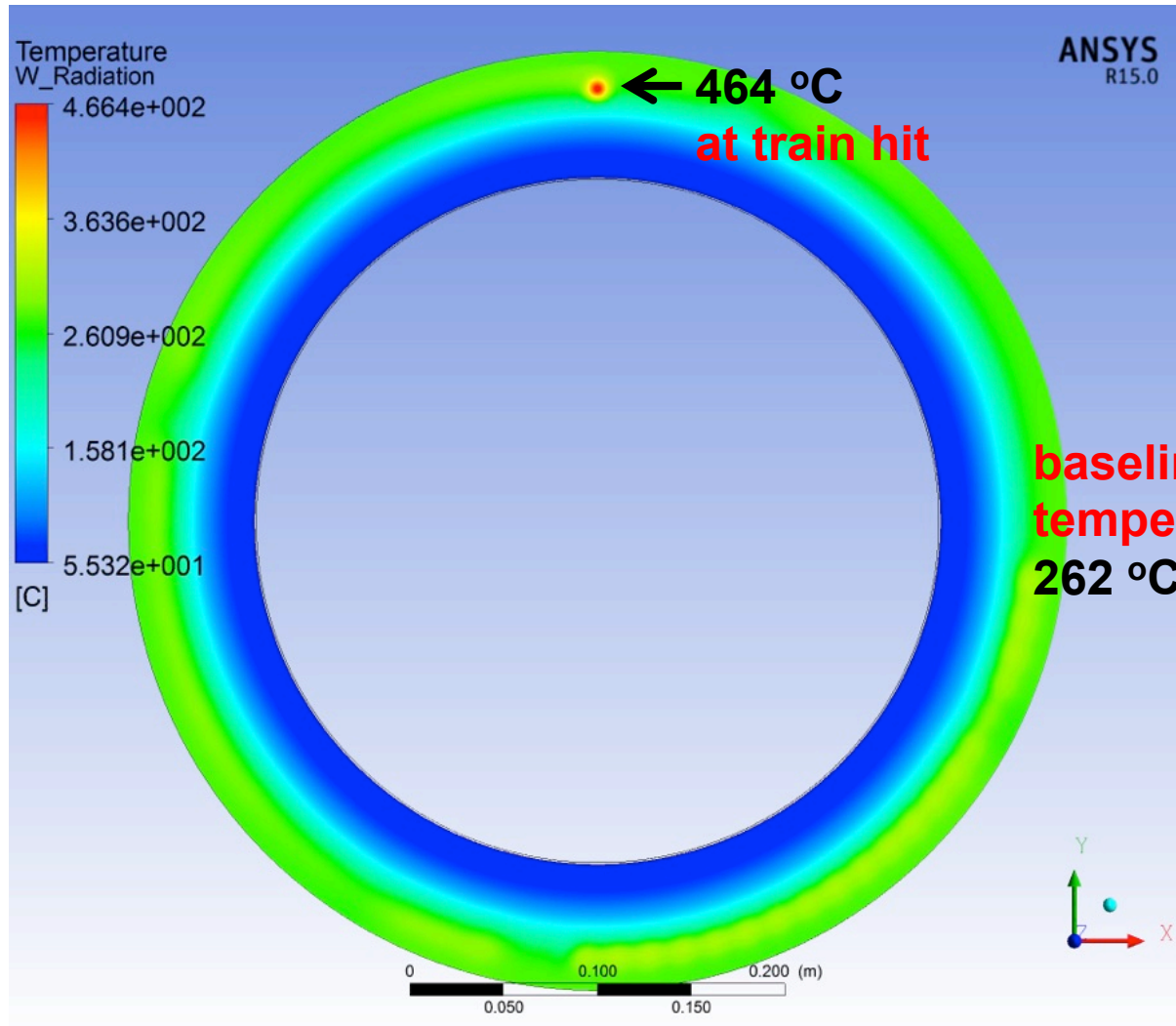
20 trains in 63 ms

1 train simulated

Rotation speed = **220rpm**

1 train = 373000 kW(**) in 0.99 micro s (*)

train to train separation: 3.3 m sec



* Note: 1

One train corresponds 132 bunches, but time structure in a train is ignored.

• Note: 2

Pulse width of a train is NOT 0.99 m sec. It is 0.99 micro sec.

We made correction

But difference in the results are small.

Corrected.

** Note: 3

This value is NOT accurate.

This is 5% larger than correct value.

Simulated by Rigaku Nb=2600

T. Omori, LCWS 2015, 3-Nov-2015, Whistler, CANADA

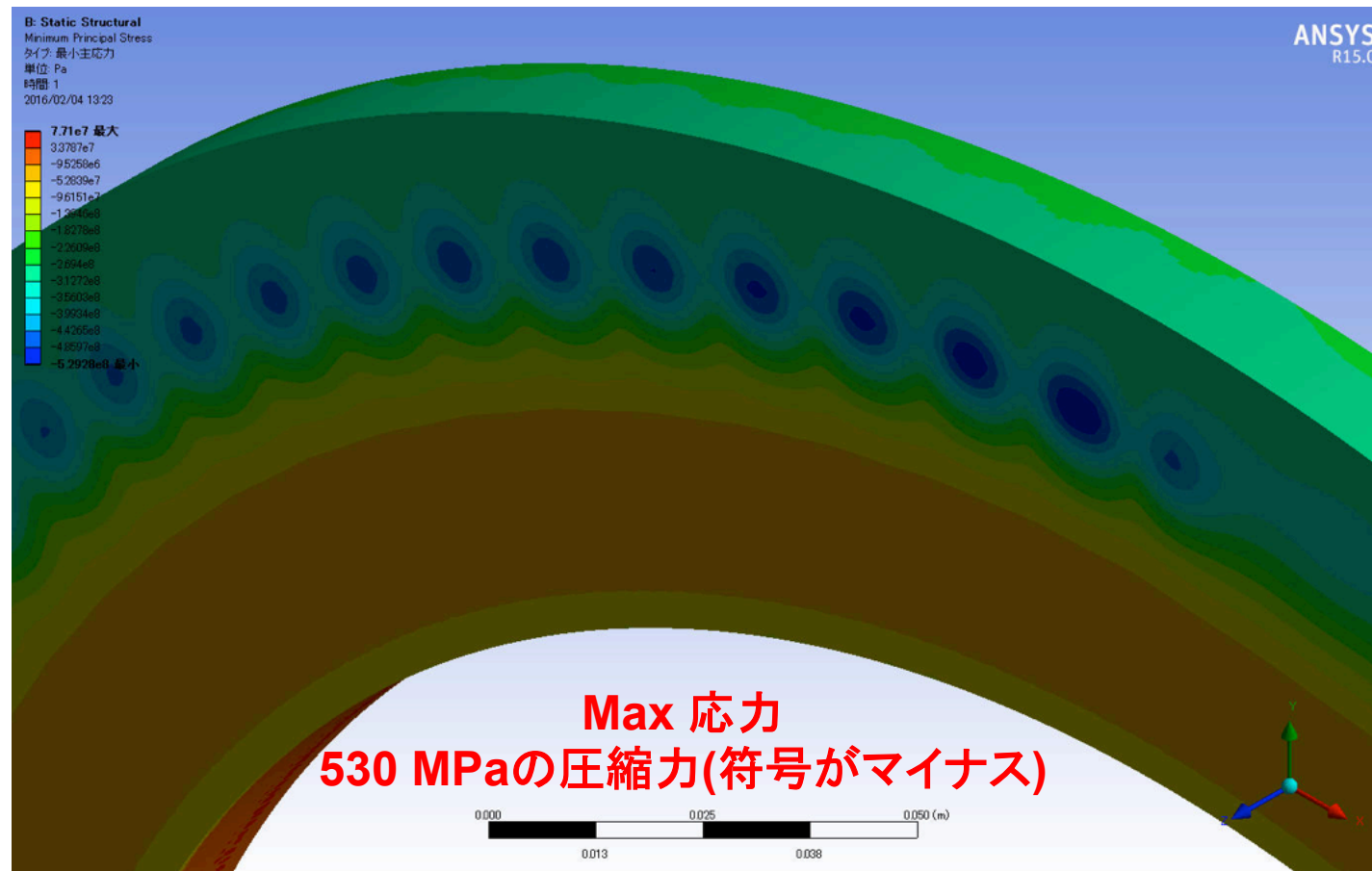
Posipol 2015 以降 (2015年9月7日以降) の解析

- (2) まず (1) の方法で十分に長い間シミュレーションし定常状態に達した後、その温度分布を
引き続いて、1 μs の間に 132 バンチがほぼ同一地点に当たる**パルスの peak** (1 μs の間)
373 MW(注1):132 バンチはまとめて**一塊=パルスとする**)をシミュレーション。

Max 435 度C (@220rpm) 前ページの場所(注3)のストレスを求める。

注3)前ページでは 466 度C となっている。
本当は 466度C であるべきだが、間違った温度分布が使われている。
ただしこのことによる差異は小さい。

山片さんの 2016年2月4日のメール
160204_Model39_3D_最小主応力_拡大.jp

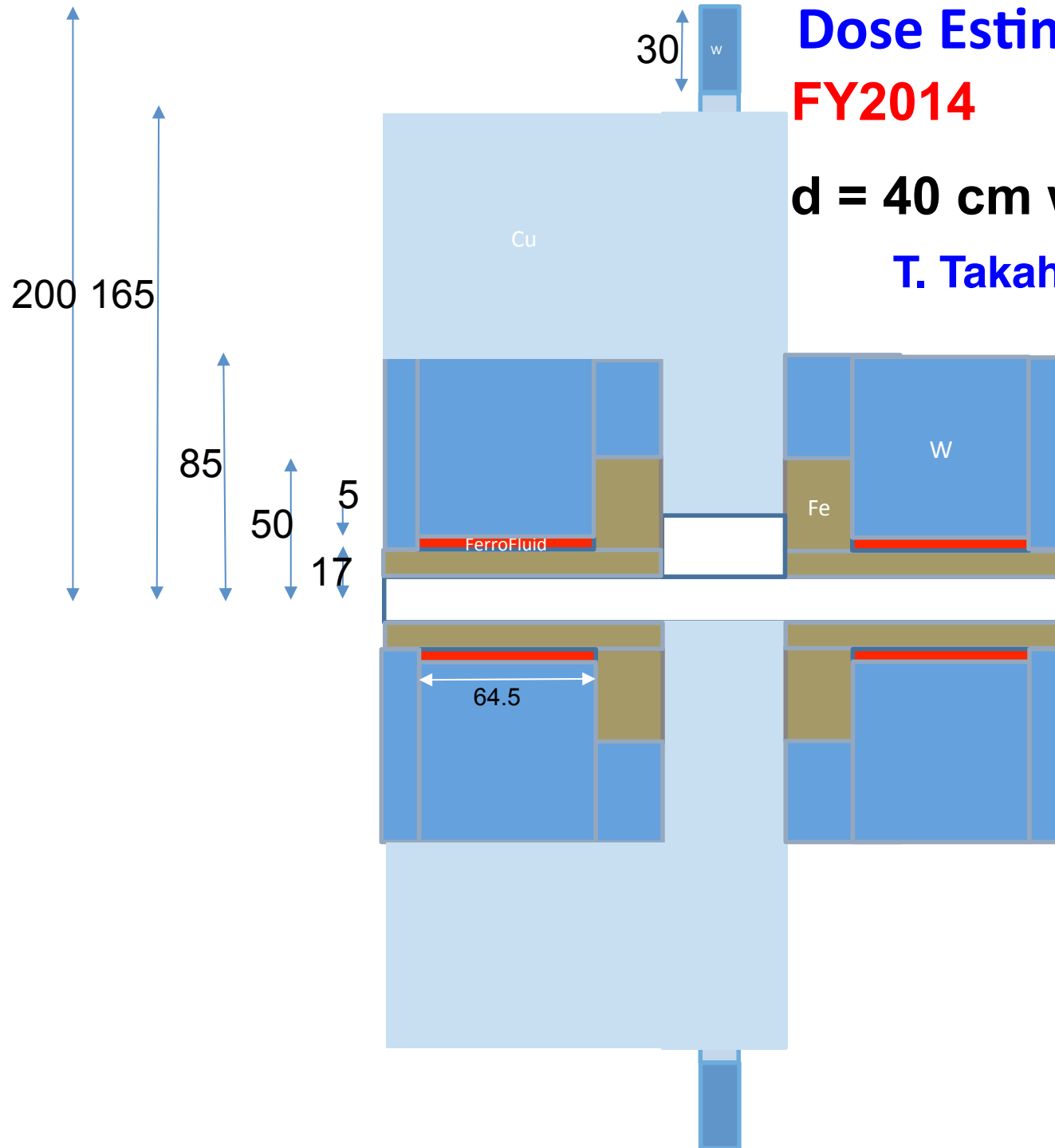


Dose Estimation

FY2014

d = 40 cm with radiation shield

T. Takahashi (Hiroshima)



Conventional e+ 源 (E-Driven) のR/D

ターゲット R/D

回転ターゲットは、類似のものが X 線発生目的で数多く作られているが、ILC 陽電子源の要求は、重量、大きさ、真空度などで、かなり異なる点がある。シミュレーションだけで十分でない部分もあり ILC がアプルーブされる前に実機大モデルの製作・実証が必要。

0. これまでに磁性流体の耐放射線試験や熱負荷、冷却、ストレスを考慮した基本設計を実施

1. 従来の計画(右図)

実機大モデル(*)を H27-H28年度 で製作

H27: **中央部製作**

H28: **ディスクと真空容器製作**

長期間運転: 真空テスト

(*) 実機大ではあるが、ディスクの材質は

W ではない、ディスクに冷却チャネルなし

2. 新しい計画(*) (広島大で 120-200 万円を用意)

小さな真空容器を作り中央部のみで真空テスト

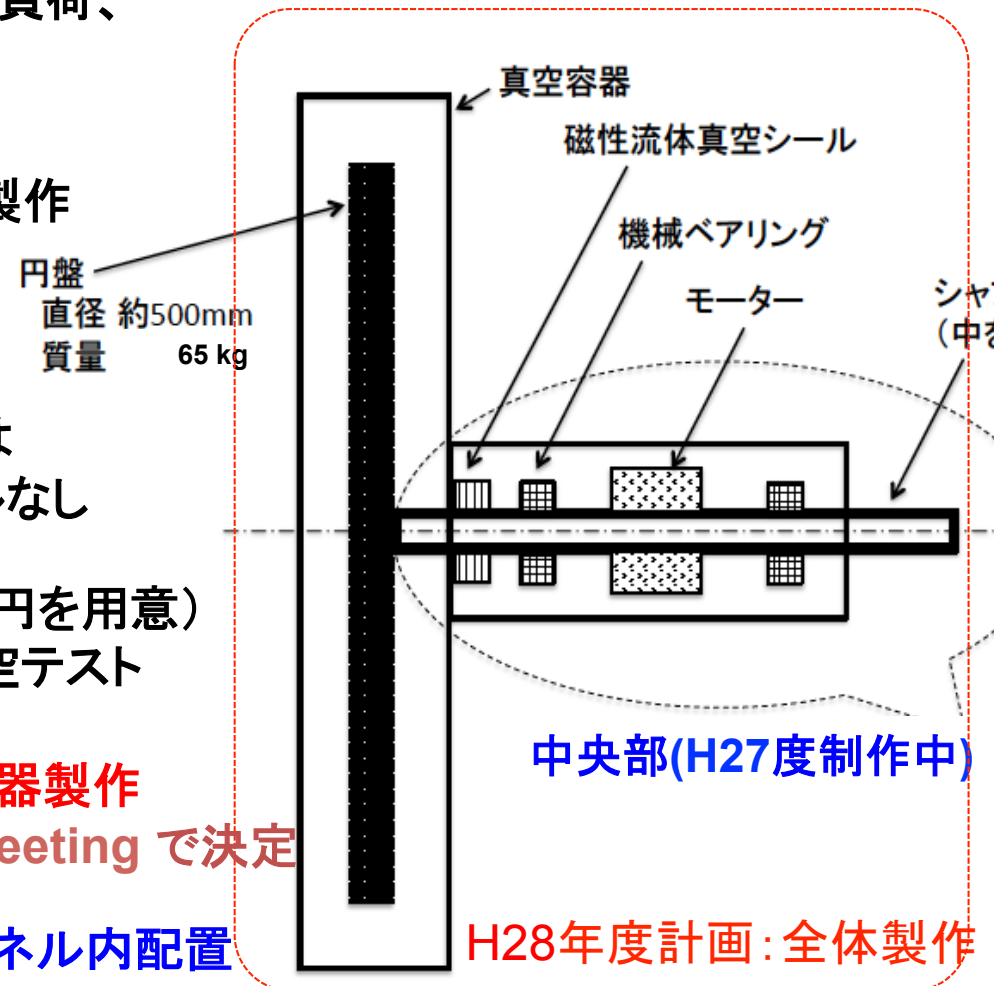
基本設計のさらなる練り上げ

補正予算がもらえれば **ディスクと真空容器製作**

* 暫定案、正式には 4/12 に 広大-KEK meeting で決定

Capture 部、5 GeV Booster、シールド、トンネル内配置

シミュレーション、図上検討を継続

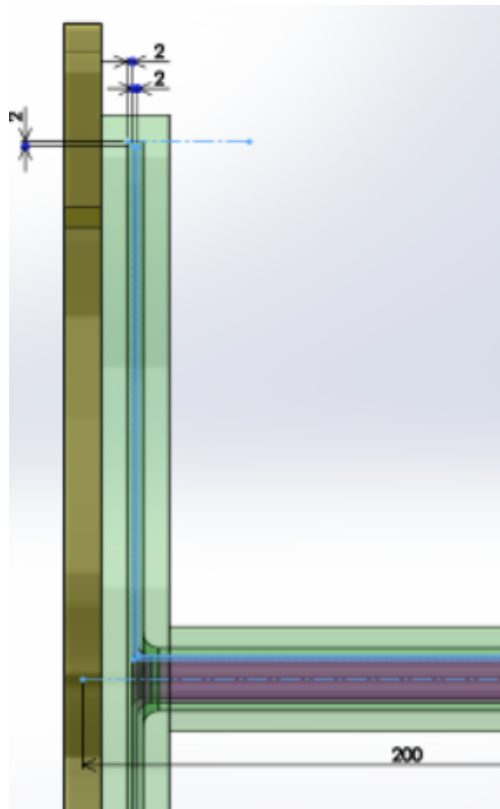


回転ターゲットプロトタイプ概略断面図

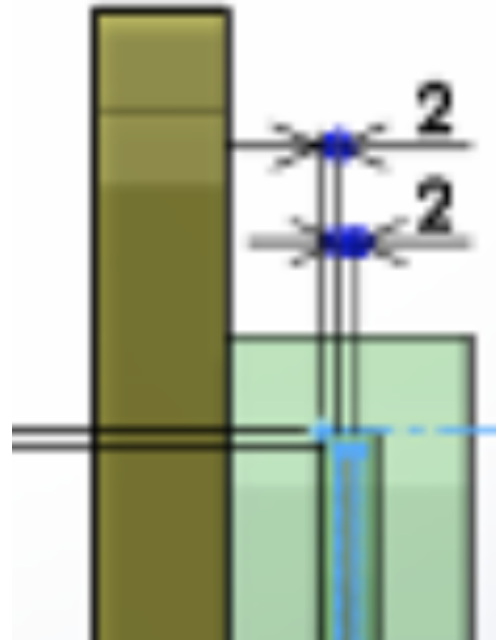
To Get Improved Safety

Trying Better Cooling: water channel design

Outline



Detail: Old Design
(Model 39)



Detail: New Design
(Model 50)

